# JV TASK 47 - DEMONSTRATION OF VACUUMENHANCED RECOVERY AND FEASIBILITY OF PERMEABLE TREATMENT BARRIERS FOR SITE REMEDIATION AT HAZEN 

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## JV TASK 47 - DEMONSTRATION OF VACUUM-ENHANCED RECOVERY AND FEASIBILITY OF PERMEABLE TREATMENT BARRIERS FOR SITE REMEDIATION AT HAZEN


#### Abstract

The Energy \& Environmental Research Center (EERC) conducted a demonstration of a vacuum-enhanced recovery and feasibility of permeable treatment barriers for soil and groundwater remediation at an Independent Oil (former Star Mart) site in Hazen, North Dakota. A total of $62,584 \mathrm{lb}(28,388 \mathrm{~kg})$ of contaminant was recovered from impacted soils and groundwater. The mass of recovered contaminant equals approximately 10,116 gallons of product. Groundwater quality monitoring confirmed the continuing contaminants of concern (COC) reduction trend in most monitoring wells and an average benzene reduction of $85 \%$ within the entire impacted area since remediation system start-up. A comparison of mass balance estimates for the extraction system with biodegradation stoichiometry using the assimilative capacity of the groundwater indicates that in situ natural attenuation processes became a dominant factor in reducing COCs and that improved site conditions justified termination of corrective action.


The unit cost of contaminant recovery was $\$ 15.26 / \mathrm{lb}$ ( $\$ 33.65 / \mathrm{kg}$ ). If in situ degradation resulting from oxygen delivery is considered, the cost would be $\$ 12.62 / \mathrm{lb}$ ( $\$ 27.82 / \mathrm{kg}$ ) of contaminant recovered or degraded.

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## EXECUTIVE SUMMARY

At the request of North Dakota Department of Health (NDDH), the Energy \& Environmental Research Center (EERC) conducted a demonstration of vacuum-enhanced recovery and investigated the feasibility of permeable treatment barriers for soil and groundwater remediation at an Independent Oil (former Star Mart) site in Hazen, North Dakota.

A total of $6,707,299$ gallons $\left(25,387 \mathrm{~m}^{3}\right.$ ) of groundwater and 110.8 million $\mathrm{ft}^{3}$ ( 3.1 million $\mathrm{m}^{3}$ ) of soil vapor have been extracted from well fields since extraction start-up, resulting in removal of over $62,584 \mathrm{lb}(28,388 \mathrm{~kg})$ of hydrocarbons prior to stripping and an additional 725 lb ( $329 \mathrm{~kg} \mathrm{)} \mathrm{from} \mathrm{the} \mathrm{treated} \mathrm{groundwater}$. approximately $10,116 \mathrm{gal}(38,290 \mathrm{I})$ of product, assuming specific gravity for gasoline of $0.75 \mathrm{~g} / \mathrm{cm}^{3}$.

Groundwater quality monitoring confirmed the continuing contaminants of concern (COC) reduction trend in most monitoring wells and an average benzene reduction of $85 \%$ within the entire impacted area since remediation system start-up. Comparison of mass balance estimates for the extraction system with biodegradation stoichiometry using the assimilative capacity of the groundwater indicates that in situ natural attenuation processes became a dominant factor in COC reduction. Improved site conditions and a steadily declining concentration of COCs justified termination of the corrective action.

The cost of contaminant recovery was $\$ 15.26 / \mathrm{lb}$ ( $\$ 33.65 / \mathrm{kg}$ ). If in situ degradation resulting from oxygen delivery is considered, the cost would be $\$ 12.62 / \mathrm{lb}$ ( $\$ 27.82 / \mathrm{kg}$ ) of contaminant recovered or degraded.

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### 1.0 INTRODUCTION

At the request of North Dakota Department of Health (NDDH), the Energy \& Environmental Research Center (EERC) conducted a demonstration of vacuum-enhanced recovery and investigated the feasibility of permeable treatment barriers for soil and groundwater remediation at an Independent Oil (former Star Mart) site in Hazen, North Dakota.

The overall objective of the project activities was to design, implement, and operate a vacuum-enhanced recovery/multiphase extraction (MPE) system to reduce contaminant concentration levels in soils and groundwater at the subject site at Hazen, North Dakota, below acceptable regulatory limits or to levels that would allow for natural attenuation processes to complete in situ degradation of residual contaminants.

Characteristics of the target zone required the application of remediation technology capable of simultaneously removing contaminants in both the vapor and liquid phases. Based on favorable results from other sites in the state and after evaluation of alternative technologies, MPE was recommended as the technically most feasible option capable of achieving high contaminant removal rates from the target zone using a combination of extraction well fields while controlling the contaminant migration off-site. The project was initiated in April 2002. The MPE system was operated from July 12, 2002, to November 22, 2005. In addition to contaminants of concern (COC) recovery, plume interception using reinjection of the treated aerated water in the permeable treatment barrier was conducted from June to October 2004 and 2005 to accelerate the in situ biodegradation process.

This report presents a summary of results including a description of the technology applied. More detailed information, original data sets, and primary documentation are compiled in technical progress reports provided to the sponsors and regulatory agency on a quarterly basis. The project was sponsored by North Dakota Petroleum Tank Release and Compensation Fund (NDPTRCF) and the U.S. Department of Energy (DOE) and supervised by NDDH.

### 2.0 EXPERIMENTAL

EERC demonstration of the MPE system as one of the most efficient technologies for site remediation and reinjection of aerated treated water into a permeable treatment barrier marked the first application of a combination of these technologies in the state of North Dakota.

Definition of the contaminated target zone, contaminant properties, and the previous remediation effort indicated that remediation technology or a combination of technologies suitable for the subject site must be capable of:

- Efficiently removing contaminants from both the vadose and saturated zones in heterogeneous sediments with relatively low permeability.
- Creating a hydraulic impact that would reduce/control free product (FP) and contaminant migration off-site.
- Being flexible enough to address water table fluctuation across the contaminant smear zone.
- Providing for oxygen supply to stimulate biodegradation.
- Providing oxygen supply to permeable treatment barrier intercepting the plume to stimulate in situ contaminant degradation processes.

Additional objectives and requirements for this demonstration were:

- A simple design to minimize operational and maintenance costs.
- Well field design that would not be disruptive to daily operation of facilities at the site.
- Demonstration of an extraction and treatment system capable of successful continuous operation in the harsh conditions dominating winter weather in North Dakota.
- Real-time system monitoring using telemetric controls to allow for flexible evaluation of remediation system parameters and timely optimization.


### 3.0 RESULTS AND DOCUMENTATION

### 3.1 Site Characteristics

### 3.1.1 Location and Release History

The subject site is located at abandoned Independent Oil, Inc., formerly Star Mart, at 334 Antelope Drive, Hazen, North Dakota, T144N R86W Section 7, Mercer County, and covers an area of approximately 2.2 acres (Figure 1 and Appendix A).

The release of an estimated $36,000 \mathrm{gal}$ of gasoline was documented in inventory records from October 1992 to August 1993; however, the reliability of the estimate could not be independently verified.

### 3.1.2 Hydrogeology and Contaminant Transport

The shallow groundwater flow and downgradient contaminant migration is bound to heterogeneous sandy silts, clayey silts, and clays of glaciofluvial origin, with construction fill in the center of the site. Abandoned channels of meandering Antelope Creek developed in discrete patterns throughout the site and likely provided preferential pathways for contaminant transport off-site and toward the current stream of Antelope Creek (Figure 1).

The unconfined water table at the subject site ranged from $2.44 \mathrm{ft}(\mathrm{MW}-6)$ to 10.54 ft (MW-7) below ground on July 10, 2002, with the mean depth to water at the center of the source area at about 9 ft . A declining trend and wide range of fluctuation in individual monitoring and extraction wells in response to operation of the extraction system were recorded during operation (Section 2.2.6). Groundwater flows across the site to the south-southeast, with an average gradient of about 0.006 (Appendix C).

Hydraulic properties reflect on geologic changes associated with a dynamic fluvial sedimentary environment, with more permeable sandy silts (hydraulic conductivity of $5.6 \times 10^{-3} \mathrm{ft} / \mathrm{min}\left[3 \times 10^{-5} \mathrm{~m} / \mathrm{s}\right]$ and a sustained yield of over 5 gpm for well MW-3) in the western part of the site and an increasing presence of clayey silts accompanied by a declining share of sands toward its eastern portion $\left(7.9 \times 10^{-4} \mathrm{ft} / \mathrm{min}\left[4 \times 10^{-6} \mathrm{~m} / \mathrm{s}\right]\right.$ and $1-\mathrm{gpm}$ yield for well MW-2).


Hazen, North Dakota


Figure 1. Site plan.

### 3.2 Remediation System

### 3.2.1 Extraction, Monitoring, and Injection Well Fields

Extraction and monitoring well field construction on June 24-27, 2002, included completion of eight (8) extraction wells and the addition of seven (7) new monitoring wells, as well as the retrofit of four (4) existing wells to allow for vacuum pressure and water level monitoring. Extraction well boreholes were advanced by a 6 -in.-i.d. (10-in.-o.d.) hollowstem auger. Wells were completed with 4-in.-diameter flush-threaded Schedule 40 PVC with a $0.020-$ in. slot screen and No. 30 red flint pack. Extraction wells are equipped with pitless adaptors installed approximately 4 ft below the ground, with $1-\mathrm{in}$. PVC suction tubes extending 4 ft below the water table (at the time of construction). Seven monitoring wells were advanced using a 4 -in.-i.d. by 8 -in.-o.d. hollowstem auger and completed as 2 -in.-diameter flush-threaded PVC, Schedule 40 PVC groundwater-monitoring wells. All extraction and selected monitoring wells were further equipped with pressure- and water-table-monitoring ports with a $3 / 4-\mathrm{in}$. drop tube extending to $<1 \mathrm{ft}$ from the bottom of the well.

The 110 -foot injection curtain completed July $7-10,2004$, consisted of 2 -in. slotted ( 0.064 slot) Schedule 40 PVC pipe, with a manifold line above. Flow could be manipulated through a series of valves along the manifold line. The slotted pipe was contained within a $15-\mathrm{in}$. bed of $3 / 4-\mathrm{in}$. washed rock; the total depth of the trench was 3 feet below ground surface. Highly oxygenated discharge water from the MPE system was injected into the curtain to intercept potential contaminant migration toward Antelope Creek. Treated discharged water from the extraction well fields met applicable criteria for benzene, toluene, ethylbenzene, and xylenes (BTEX) prior to reinjection. Figure 1 presents the site plan; the site layout is given in Appendix A.

Well completion technical data including geologic and survey logs are provided in Technical Progress Reports for April - July 2002 [1]. Following NDDH and EERC agreement on final activities at the site from June 13, 2006, all extraction and monitoring wells including piping and manifolds in ground were sealed June 19-22, 2006, in compliance with Article 33-18 North Dakota Administrative Code (NDAC) and NDDH guidelines for well abandonment.

### 3.2.2 Dual-Phase Extraction and Treatment System

The extraction and treatment system consists of a CoVac-500" 4-stage, 25-hp, oil-free regenerative blower with a maximum rating of 250 acfm @ $24 \mathrm{in} . \mathrm{Hg}$. Recovered water and air pass through the 60-gal vapor-liquid separator (VLS) to the Hydro-Flo model TST-8 oil-water separator (OWS) with an integrated product storage tank. Water from the OWS is then pumped to a six-stage LP-2.6P air stripper (AS). Seasonally, with warm air temperatures, water from the AS is conveyed to an injection curtain which was installed on July 7-10, 2004 (Figure 1). The system layout and process flow design are provided in Appendix B.

The extraction and treatment system is equipped with a NEMA 4 controller, modem, and telemetry package, allowing for both on-site and telemetric control of the power circuits including monitoring of system performance parameters. Basic operational parameters are summarized in Table 1.

## Table 1. Operational Parameters

| Well Field | HR- 1, 2, 3, 4, 5, 6, 7, 8 |
| :--- | :---: |
| Operated (date) | $7 / 11 / 02-11 / 22 / 05$ |
| Groundwater Flow (gpm - average/range) | $5.9 / 0.4-11.4$ |
| Combined Airflow (cfm - average/range) | $90 / 50-153$ |
| Inlet Vacuum (in. Hg - average/range) | $14.5 / 8-19$ |
| Extraction Wellhead Vacuum (in. $\mathrm{H}_{2} \mathrm{O}$ - average/average range) | $65 / 30-111$ |
| Total Operating Hours (runtime-h) | 19,889 |
| Operating efficiency1 7/11/02-11/22/05 | $90.4 \%$ |

${ }^{1}$ Downtime includes all maintenance shutdowns except for winter pauses.

### 3.2.3 System Performance Monitoring and Sampling

The MPE and treatment system started break-in operation on July 11, 2002. After system optimization, full-scale operation commenced October 2, 2002. System performance monitoring and effluent water and offgas sampling were conducted on a monthly basis; telemetric system control and data download was conducted daily throughout the operation. Alternating well fields were combined from up to six simultaneously operated wells integrated to maximize capture zone and contaminant removal efficiency while providing hydraulic control for off-site migration.

### 3.2.4 System Water Quality

Samples of extracted water and treated effluent were analyzed for COC (benzene, toluene, ethylbenzene, xylenes, phenols, and total petroleum hydrocarbons [TPH] as gasoline range organics [GRO]), total iron and manganese, and suspended solids. Field measured parameters included pH , electrical conductivity (EC), and temperature.

Values representing contaminant recovery from the respective well fields exhibited declining trends from TPH and BTEX values as high as $189.1 \mathrm{mg} / \mathrm{l}$ and $14.1 \mathrm{mg} / \mathrm{l}$, respectively, to nondetect before system shutdown. A summary of extraction and treatment data is provided in Appendix G-1; complete analytical documentation is in the respective technical progress reports. A 100\% water treatment system efficiency was achieved for BTEX removal.

### 3.2.5 Offgas Quality

Offgas quality from combined exhaust was monitored using charcoal tubes and real-time monitoring of hydrocarbons, $\mathrm{CO}_{2}$, and $\mathrm{O}_{2}$ using a photoionization detector (PID), a flame ionization detector (FID), and a Summit hydrocarbon analyzer.

Offgas-sampling results using charcoal tube desorption and analyzed by gas chromatography (GC)/FID are summarized in Appendix G-2. VOC concentration trends are provided in Figure 2. To overcome fluctuating airflow velocities, offgas was collected in a 1-I Tedlar bag at a rate of approximately $0.3 \mathrm{l} / \mathrm{min}$. Charcoal tube samples were subsequently collected directly from the Tedlar bag using an SKC pump with flow regulated at $0.28 \mathrm{I} / \mathrm{min}$. In addition, carbon dioxide and oxygen trends in extracted vapors were monitored using the Summit analyzer. The mass balance for recovered VOCs and average emission loads were calculated based on results of offgas analyses and average exhaust airflow corrected to standard conditions and reported to NDDH on a quarterly basis.

Extremely high volatile organic compounds (VOC) concentrations of $332,000 \mathrm{mg} / \mathrm{m}^{3}$ (TPH) and $8950 \mathrm{mg} / \mathrm{m}^{3}$ for BTEX recorded and analyzed during the first days of extraction indicated the presence of considerable amounts of residual free product trapped within the vadose and dewatered smear zone (Appendix G-2). VOCs in offgas typically sharply declined within several weeks of operation of a new well field and were mostly bellow detection limits for any combination of wells before system shutdown.

### 3.2.6 Hydraulic and Pneumatic Response

Groundwater table monitoring at the extraction and monitoring wells was conducted on a weekly basis from system start-up through October 16, 2002, and on a monthly basis from October 16, 2002, through November 22, 2005. Depth to water at the subject site ranged from near surface in well MW-6 during injection to 16.55 ft (MW-2) below ground, with the mean depth to water at the center of the source area at about 9.47 ft . Annual fluctuation of 2.633.68 ft was observed from July 10, 2002, to November 22, 2005, in hydraulically unimpacted wells MW-4, MW-7, and MW-17.

Drawdown measured at extraction wells ranged from 4.67 to 7.85 ft , with maximum values resulting in intermittent well dewatering. Average groundwater table decline within the source area during system operation was 13.58 ft below ground, yielding a $4.1-\mathrm{ft}$ drawdown, i.e., meeting design criteria that required smear zone exposure and dewatering, allowing air to be a


Run Time (h)

Figure 2. Hydrocarbon concentration trends in offgas since system start-up (initial data points exceed concentrations represented in figure).
primary contaminant carrier in the target zone. Considerable fluctuation of water levels and differences in hydraulic impact for each well are typically observed for single-pump vacuumenhanced recovery wells as a result of fluctuating vacuum levels and variability in hydraulic conductivities specific to heterogeneous sediments within the extraction well field. Water level records and vacuum-monitoring data are summarized in Appendices C and D ; detailed response maps are provided in quarterly technical progress reports.

Similarly to water table monitoring, the vacuum pressure at the extraction and monitoring wells was measured on a weekly basis until October 16, 2002, and on a monthly basis until November 22, 2005. Average operating vacuum for individual extraction wells ranged from 10.1 to $163.2 \mathrm{in} . \mathrm{H}_{2} \mathrm{O}$, with an overall average of $65 \mathrm{in} . \mathrm{H}_{2} \mathrm{O}$ (Table 1). The highest vacuums resulted in temporary dewatering of extraction wells. Vacuum recorded at monitoring wells ranged from 0.1 to $80.4 \mathrm{in} . \mathrm{H}_{2} \mathrm{O}$ (with vacuum pressure of $0.1 \mathrm{in} . \mathrm{H}_{2} \mathrm{O}$ considered a cutoff value). Pneumatic impact was observed as far as $120-140 \mathrm{ft}$ from the center of the extraction well field, with radii of influence for individual wells up to 60 ft . Vacuum-monitoring data are summarized in Appendix D, including an example map of pneumatic influence.

### 3.3 Contaminant Recovery Estimation

A total of $6,707,299$ gallons $\left(25,387 \mathrm{~m}^{3}\right.$ ) of groundwater and 110.8 million $\mathrm{ft}^{3}$ ( 3.1 million $\mathrm{m}^{3}$ ) of soil vapor have been extracted from well fields since extraction start-up, resulting in removal of over $62,584 \mathrm{lb}(28,388 \mathrm{~kg})$ of hydrocarbons prior to stripping and an additional 725 lb $(329 \mathrm{~kg})$ from the treated groundwater. The mass of recovered contaminant equals approximately $10,116 \mathrm{gal}(38,290 \mathrm{I})$ of product, assuming specific gravity for gasoline of $0.75 \mathrm{~g} / \mathrm{cm}^{3}$. The average liquid flow rate since system start-up was approximately 5.90 gpm ( $22 \mathrm{l} / \mathrm{s}$ ), ranging from 0.4 to 11.4 gpm . The average airflow rate was $90 \mathrm{scfm}\left(2.5 \mathrm{~m}^{3} / \mathrm{min}\right)$, ranging from 50 to 153 scfm , with an average temperature of $225^{\circ} \mathrm{F}\left(107^{\circ} \mathrm{C}\right)$. Data for mass removal calculation are provided in Appendix E; cumulative recovery is presented in Figures 3 and 4.

In addition to contaminant recovered by extraction and reduced by in situ biodegradation as a result of injection into a permeable treatment barrier, a total of $41,440 \mathrm{lb}(18,800 \mathrm{~kg})$ of oxygen was delivered to the contaminated zone during operation of the MPE system between July 11, 2002, and November 22, 2005, assuming 2\% oxygen transfer efficiency [2] and 110.8 million $\mathrm{ft}^{3}$ ( 3.13 million $\mathrm{m}^{3}$ ) soil vapor exchanged/recovered.

Although quantification of in situ oxygen partitioning between soil- and groundwater-bound contaminants and their subsequent reduction is extremely difficult, by providing the necessary electron acceptor and assuming that a reduction of $1 \mathrm{mg} / \mathrm{l}$ of dissolved oxygen consumed by microbes results in biodegradation of $0.32 \mathrm{mg} / \mathrm{l}$ of benzene, the volume of oxygen delivered would translate into further in situ reduction of about $13,261 \mathrm{lb}(6015 \mathrm{~kg}) \sim 2120$ gallons ( 8000 l ) of contaminant in the saturated zone.

### 3.4 Groundwater Quality Monitoring

### 3.4.1 Well Sampling

Selected monitoring and extraction wells were sampled for BTEX and biodegradation indicators on a semiannual basis to document overall remediation system impact on groundwater quality compared to original site data collected in June/July 2002 (prior to system start-up). The final sampling was conducted on May 9, 2006, 6 months after system shutdown.


Figure 3. Cumulative TPH and BTEX removal - liquid phase.


Figure 4. Total hydrocarbon removal.

Groundwater samples were collected using disposable PVC bailers, preserved on-site, and stored on ice prior to and during shipment. Samples for dissolved metals were filtered using $0.45-\mu \mathrm{m}$ Geotech disposable filters. Analyses were conducted by MVTL in Bismarck, North Dakota, and New Ulm, Minnesota. Quality assurance/quality control samples included duplicates, equipment blanks, field blanks, and trip blanks for each sampling event. Fieldmonitored water quality parameters were measured in wells with an YSI-556 multiprobe.

### 3.4.2 Water Quality Trends

Asymptotic trends, declining VOC concentrations, and mass recovery efficiency in groundwater and soil vapor extracted between system start-up (July 2001) and November 2005 indicate that most of the residual FP trapped within the vadose and dewatered smear zone has been successfully removed, and further contaminant release is rate-limited (Figures 2 and 3, and mass balance worksheets in Appendix E).

Analytical results from the most recent sampling indicate that an overall 79\% BTEX and 85\% benzene reduction in groundwater was achieved since June 2002 (prior to system start-up) and that most of the contaminant plume is already amenable to natural biodegradation (Table 2). While concentrations of benzene and GRO remain above regulatory limits in several contaminated wells, concentrations of toluene, ethylbenzene, and xylene in most wells were successfully reduced to regulatorily acceptable limits of $1000 \mathrm{ppb}, 700 \mathrm{ppb}$, and $10,000 \mathrm{ppb}$, respectively. BTEX was reduced to near- or nondetect levels in wells MW-2, 3, 11, 13, and 17. The summary of groundwater analyses before system start-up and 6 months after shutdown is provided in Table 3.

Declining trends and COC reduction of about 50\% and 20\% are documented for wells MW-10 and MW-16, respectively. Because of their location in a clayey sediment profile, both wells persistently exhibited relatively high concentrations of COC. A significant recent COC increase documented in well MW-12 since November 22, 2005, is in contrast to previous $98 \%$ COC reduction until May 4, 2005 (Appendix F-1). A comparison of the chromatographic signature of the groundwater samples from this well with other wells at the site is indicative of fresh gasoline and suggests recent incidental release directly to the well located in the middle of the frequented parking lot. Considerable COC reduction achieved as a result of corrective action and high risks associated with potential for secondary contamination prompted NDDH decision to proceed with abandonment of all wells at the site.

Table 2. Contaminant Reduction (average from all contaminated wells)

|  | COC Reduction (\%) |  |
| :--- | :--- | :--- |
| BTEX | 79 | $85^{*}$ |
| Benzene | 85 | $94^{*}$ |
| GRO | 81 | $85^{*}$ |

*MW-12 data excluded.

Table 3. Groundwater Analyses - COC

| Well ID | Date | $\begin{gathered} \text { Benzene } \\ \text { ppb } \end{gathered}$ | Toluene ppb | Ethylbenzene ppb | Xylenes (total) ppb | GRO (TPH) mg/l | $\begin{gathered} \text { BTEX } \\ \text { ppb } \\ \hline \end{gathered}$ | BTEX Trend |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MW-1 | 04/08/02 | 34000 | 7790 | 2200 | 6440 | 133.0 | 50430 | $\nabla$ |
| MW-1 | 05/09/06 | 978 | 56.6 | 1284 | 1194 | 16.2 | 3513 |  |
| MW-2 | 04/09/02 | 4010 | 326 | 305 | 752 | 16.3 | 5393 |  |
| MW-2 | 05/09/06 | 12.5 | <1 | 3.4 | 5.7 | $<0.2$ | 22 |  |
| MW-3 | 04/09/02 | 777 | 1240 | 77.3 | 636 | 7.3 | 2730 |  |
| MW-3 | 05/09/06 | <1 | $<1$ | <1 | <3 | <0.2 | 0 |  |
| MW-4 | 04/08/02 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-4 | 05/09/06 | <1 | <1 | $<1$ | <3 | <0.2 | 0 |  |
| MW-5 | 04/08/02 | 30000 | 4000 | 584 | 977 | 101.0 | 35561 |  |
| MW-5 | 05/09/06 | 4754 | 1817 | 2417 | 2807 | 31.3 | 11795 |  |
| MW-6 | 04/08/02 | 11100 | <100 | 213 | <300 | 28.0 | 11313 | $\nabla$ |
| MW-6 | 05/09/06 | 209.5 | 1.6 | 58 | 3.6 | 1.5 | 269 |  |
| MW-7 | 04/08/02 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-7 | 05/09/06 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-8 | 04/08/02 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-8 | 05/09/06 | <1 | $<1$ | <1 | <3 | <0.2 | 0 |  |
| MW-9 | 04/08/02 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-9 | 11/22/05 | <1 | $<1$ | <1 | <3 | <0.2 | 0 |  |
| MW-10 | 04/08/02 | 52800 | 16600 | 1470 | 4160 | 167.0 | 75030 |  |
| MW-10 | 05/09/06 | 5696 | 13940 | 2850 | 13360 | 71.9 | 35846 |  |
| MW-11 | 07/23/02 | 5310 | 14100 | 1920 | 12500 | 107.0 | 33830 |  |
| MW-11 | 05/09/06 | <1 | $<1$ | <1 | <3 | <0.2 | 0 |  |
| MW-12 | 07/23/02 | 34700 | 29200 | 2180 | 9940 | 163.0 | 76020 |  |
| MW-12 | 05/09/06 | 36750 | 19340 | 1426 | 7937 | 100.8 | 65453 |  |
| MW-13 | 07/10/02 | 47900 | 21900 | 2590 | 9970 | 201.0 | 82360 |  |
| MW-13 | 05/09/06 | 37.7 | <2 | 117.9 | 24.5 | 1.8 | 180 |  |
| MW-14 | 07/23/02 | 34400 | 36300 | 3260 | 17100 | 209.0 | 91060 |  |
| MW-14 | 05/09/06 | 2441 | 21.7 | 777.2 | 274.8 | 10.7 | 3515 |  |
| MW-15 | 07/23/02 | 31900 | 27700 | 2610 | 10700 | 174.0 | 72910 |  |
| MW-15 | 05/09/06 | 844 | 1692 | 1516 | 7963 | 29.6 | 12015 | $\nabla$ |
| MW-16 | 07/10/02 | 26400 | <250 | 304 | <750 | 52.1 | 26704 |  |
| MW-16 | 05/09/06 | 19130 | 133.6 | 1233 | 177.4 | 34.2 | 20674 | $\nabla$ |
| MW-17 | 07/10/02 | 11.9 | 3 | <1 | <3 | <0.2 | 15 |  |
| MW-17 | 05/09/06 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |

Evaluation of natural attenuation conditions was carried out in order to determine the potential for further in situ reduction of COC levels in soil and groundwater. Although some biodegradation indicators exhibit trends typical for a contaminant plume with suppressed nitrate, dissolved oxygen (DO), and higher concentrations of manganese and ferrous iron, the plume exhibits marginal characteristics representative more of a transition between aerobic to anaerobic conditions.

In addition to trend analyses based on consistently declining COC concentrations in monitoring wells, evaluation of the aquifer's assimilative capacity was carried out to assess the aquifer's ability to complete BTEX degradation. The assimilative capacity assumes instantaneous degradation of BTEX once the contaminant is in contact with the primary electron acceptors (dissolved oxygen, nitrate, ferric iron, and sulfate). The assimilative capacity of the
groundwater calculated at $18.2 \mathrm{mg} / \mathrm{I}$ (based on May 9, 2006, conditions) exceeds the concentrations of residual BTEX in most wells, with exception of wells MW-10, 12, and 16. Under current conditions, most of the aquifer is capable of completing the natural biodegradation process, but an excess of carbon (contaminants) in areas around the noted wells including a deficit of electron acceptors reduces biodegradation potential.

### 3.5 Technical and Economic Summary and Discussion

The MPE system was successfully operating $90 \%$ of the time, including monthly maintenance shutdowns, between July 11, 2001, and November 22, 2005. Excluded are winter pauses from January to March requested by the City of Hazen to reduce potential for effluent freezeup in a discharge ditch.

High contaminant removal efficiency of dual-phase (multiphase) extraction technology is a result of a combination of simultaneous extraction of water and vapor. It follows from contaminant recovery/degradation breakdown estimates (Table 4) that vapor extraction efficiency by far exceeds that for groundwater (in this case by a factor of 86) and, to a certain extent, draws a comparison between soil vapor extraction and pump-and-treat systems. Documented high contaminant recovery using vapor as a primary carrier could not, however, be achieved without simultaneous dewatering of the targeted smear zone.

Table 4. Contaminant recovery/degradation breakdown estimates

| COC Recovered/Degraded | Total |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | ( lb) | $(\mathbf{k g})$ | (gal) | (\%) |
| Vapor extraction | 62,584 | 28,388 | 10,000 | 81.7 |
| Groundwater extraction | 725 | 329 | 116 | 1 |
| Degradation by air exchange $/ \mathrm{O}_{2}$ delivery | 13261 | 6015 | 2119 | 17.3 |
|  | 76570 | 34732 | 12235 | 100 |

An additional advantage of dual-phase extraction is air exchange/oxygen delivery to the contaminated zone during operation of the MPE system. Because quantification of in situ oxygen partitioning between soil- and groundwater-bound contaminants and their subsequent reduction is extremely difficult, this means of degradation, albeit substantial, is often not considered by the environmental industry in mass balance estimates.

Based on project cost and total contaminant recovery of 63, 309 lb per unit, the cost for contaminant recovery was $\$ 15.26 / \mathrm{lb}$ ( $\$ 33.65 / \mathrm{kg}$ ). If in situ degradation resulting from oxygen delivery is considered, the cost would be $\$ 12.62 / \mathrm{lb}(\$ 27.82 / \mathrm{kg})$ of contaminant recovered/degraded.

### 4.0 CONCLUSIONS

A total of $6,707,299$ gallons $\left(25,387 \mathrm{~m}^{3}\right)$ of groundwater and 110.8 million $\mathrm{ft}^{3}$ ( 3.1 million $\mathrm{m}^{3}$ ) of soil vapor have been extracted from well fields since extraction start-up, resulting in removal of over $62,584 \mathrm{lb}(28,388 \mathrm{~kg})$ of hydrocarbons prior to stripping and an additional $725 \mathrm{lb}(329 \mathrm{~kg})$ from the treated groundwater. The mass of recovered contaminant equals approximately $10,116 \mathrm{gal}(38,290 \mathrm{I})$ of product, assuming specific gravity for gasoline of $0.75 \mathrm{~g} / \mathrm{cm}^{3}$.

Analytical results from the most recent sampling indicate that about $83 \%$ average improvement in groundwater quality was achieved since June 2002 (prior to system start-up) and that most of the contaminant plume is already amenable to natural biodegradation. With exception of benzene, concentrations of toluene, ethylbenzene, and xylene in most wells were successfully reduced to regulatorily acceptable limits of $1000 \mathrm{ppb}, 700 \mathrm{ppb}$, and $10,000 \mathrm{ppb}$, respectively.

Groundwater quality monitoring confirmed the continuing COC reduction trend in most monitoring wells and an average benzene reduction of $85 \%$ within the entire impacted area since remediation system start-up. Comparison of mass balance estimates for the extraction system with biodegradation stoichiometry using the assimilative capacity of the groundwater indicates that in situ natural attenuation processes became a dominant factor in COC reduction. Improved site conditions justified termination of corrective action.

The cost of contaminant recovery was $\$ 15.26 / \mathrm{lb}$ ( $\$ 33.65 / \mathrm{kg}$ ). If in situ degradation resulting from oxygen delivery is considered, the cost would be $\$ 12.62 / \mathrm{lb}$ ( $\$ 27.82 / \mathrm{kg}$ ) of contaminant recovered or degraded.

### 5.0 REFERENCES

1. Solc, J., 2002, Demonstration of vacuum-enhanced recovery and feasibility of permeable treatment barriers for site remediation at Hazen: Progress Report for April-July 2002.
2. Kuo, J., 1999, Practical Design Calculations for Groundwater and Soil Remediation. CRC Press, LLC Lewis Publishers, Boca Raton, Florida.

## APPENDIX A

## SITE PLAN AND EXTRACTION WELL FIELD



## APPENDIX B

## MPE AND TREATMENT SYSTEM



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## APPENDIX C

## HYDRAULIC RESPONSE - DATA SUMMARY AND GROUNDWATER TABLE CONFIGURATION


Groundwater Table Monitoring
Elevations in feet

| Well ID | Ground | TOC | MP1 | 07/10/02 | 07/12/02 | 07/16/02 | 07/23/02 | 07/31/02 | 08/07/02 | 08/15/02 | 08/23/02 | 09/05/02 | 09/18/02 | 09/23/02 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HR-1 | 1749.70 | 1748.99 | 1749.20 | 1742.08 | 1741.29 | 1741.30 | 1741.57 | 1741.48 | 1741.43 | 1740.86 | 1740.58 | 1741.07 | 1740.90 | 1740.36 |
| HR-2 | 1749.29 | 1748.79 | 1748.98 | 1742.14 | 1734.27 | 1734.26 | 1734.28 | 1734.28 | 1734.31 | 1734.14 | 1734.88 | <1734.14 | <1734.14 | <1734.14 |
| HR-3 | 1750.72 | 1750.17 | 1750.36 | 1742.12 | 1735.20 | 1735.11 | 1735.11 | 1735.12 | 1735.16 | 1741.31 | 1741.31 | <1735.15 | <1735.15 | <1735.15 |
| HR-4 | 1750.85 | 1750.25 | 1750.44 | 1742.17 | 1735.18 | 1735.17 | 1735.12 | 1735.14 | 1735.29 | 1735.10 | 1735.58 | <1735.29 | <1735.29 | <1735.29 |
| HR-5 | 1752.27 | 1751.62 | 1751.83 | 1742.28 | 1736.63 | 1736.62 | 1736.53 | 1736.54 | 1736.73 | 1736.54 | 1736.91 | <1736.72 | <1736.72 | <1736.72 |
| HR-6 | 1751.10 | 1750.47 | 1750.68 | 1742.18 | 1740.58 | 1741.93 | 1741.98 | 1741.99 | 1741.64 | 1741.53 | 1741.23 | 1741.36 | 1741.22 | 1741.13 |
| HR-7 | 1752.26 | 1751.50 | 1751.71 | 1742.30 | 1742.00 | 1741.87 | 1741.81 | 1741.81 | 1741.86 | 1741.52 | 1741.85 | 1741.55 | 1741.04 | 1741.26 |
| HR-8 | 1751.37 | 1750.71 | 1750.93 | 1742.22 | 1742.02 | 1741.88 | 1741.93 | 1741.94 | 1741.92 | 1741.54 | 1741.20 | 1741.60 | 1741.55 | 1741.31 |

[^0]Groundwater Table Monitoring
Elevations in feet

| Well ID | $10 / 02 / 02$ | $10 / 16 / 02$ | $11 / 18 / 02$ | $12 / 16 / 02$ | $01 / 07 / 03$ | $02 / 18 / 03$ |
| :---: | ---: | ---: | ---: | ---: | :---: | :---: |
| HR-1 | 1740.18 | 1740.39 | 1740.28 | 1740.36 | 1740.46 | NM |
| HR-2 | $<1734.14$ | $<1734.14$ | $<1734.14$ | $<1734.14$ | $<1734.14$ | 1740.68 |
| HR-3 | $<1735.15$ | $<1735.15$ | $<1735.15$ | $<1735.15$ | $<1735.15$ | NM |
| HR-4 | $<1735.29$ | $<1735.29$ | $<1735.29$ | $<1735.29$ | $<1735.29$ | 1740.95 |
| HR-5 | $<1736.72$ | $<1736.72$ | $<1736.72$ | $<1736.72$ | $<1736.72$ | 1741.02 |
| HR-6 | 1740.96 | 1741.04 | 1740.90 | 1740.88 | 1740.85 | NM |
| HR-7 | 1741.06 | 1741.15 | 1740.89 | 1740.84 | 1740.81 | 1741.07 |
| HR-8 | 1741.10 | 1741.18 | 1741.04 | 1740.99 | 1740.94 | 1741.10 |


| MW-1 | 1740.28 | 1740.36 | 1740.23 | 1740.14 | 1740.08 | 1740.40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MW-2 | 1739.75 | 1739.43 | 1738.71 | 1738.33 | 1738.55 | 1740.82 |
| MWW-3 | 1741.09 | 1741.18 | 1741.02 | 1740.91 | 1740.88 | 1741.05 |
| MW-4 | 1741.57 | 1741.59 | 1741.07 | 1741.26 | 1741.22 | 1741.20 |
| MW-5 | 1740.91 | 1741.14 | 1740.72 | 1741.07 | 1741.35 | 1740.62 |
| MW-6 | 1739.12 | 1739.46 | 1739.41 | 1739.34 | 1739.46 | 1739.01 |
| MW-7 | 1741.69 | 1741.67 | 1741.50 | 1741.38 | 1741.31 | NM |
| MW-8 | 1741.20 | 1741.25 | 1741.12 | 1741.05 | 1741.03 | 1741.12 |
| MW-9 | 1740.52 | 1740.64 | 1740.57 | 1740.52 | 1740.53 | NM |
| MW-10 | 1737.91 | 1738.17 | 1738.38 | 1738.47 | 1738.51 | 1740.52 |
| MW-11 | 1741.12 | 1741.19 | 1741.03 | 1740.92 | 1740.88 | 1741.01 |
| MW-12 | 1741.07 | 1741.23 | 1741.05 | 1740.96 | 1740.93 | 1741.03 |
| MW-13 | 1740.87 | 1740.96 | 1740.82 | 1740.96 | 1740.74 | 1740.91 |
| MW-14 | 1740.78 | 1740.86 | 1740.74 | 1740.69 | 1740.68 | 1740.94 |
| MW-15 | 1740.51 | 1740.65 | 1740.50 | 1740.44 | 1740.42 | 1741.15 |
| MW-16 | 1740.01 | 1740.26 | 1740.17 | 1740.18 | 1740.30 | NM |
| MW-17 | 1738.71 | 1739.47 | 1739.01 | 1738.94 | 1739.39 | 1738.47 |

Groundwater Table Monitoring
Elevations in feet

| Well ID | $03 / 27 / 03$ | $03 / 28 / 03$ | $04 / 23 / 03$ | $05 / 19 / 03$ | $06 / 17 / 03$ | $07 / 15 / 03$ | $08 / 21 / 03$ | $09 / 23 / 03$ | $10 / 22 / 03$ | $11 / 17 / 03$ | $12 / 17 / 03$ |
| :---: | ---: | ---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| HR-1 | 1740.75 | $<1734.44$ | NM | 1734.47 | 1740.79 | 1740.75 | 1737.57 | 1740.27 | 1739.13 | 1742.32 | 1739.79 |
| HR-2 | 1740.79 | $<1734.14$ | NM | 1734.35 | 1734.31 | $<1734.14$ | 1735.54 | 1737.93 | 1739.41 | 1739.70 | 1734.50 |
| HR-3 | 1736.11 | $<1735.15$ | NM | 1735.61 | $<1735.15$ | $<1735.15$ | 1740.40 | 1740.36 | 1739.90 | 1740.54 | NM |
| HR-4 | 1740.94 | $<1735.29$ | NM | 1735.36 | $<1735.29$ | $<1735.29$ | 1735.29 | 1735.19 | dry | dry | dry |
| HR-5 | 1741.05 | $<1736.72$ | NM | 1736.75 | $<1736.72$ | $<1736.72$ | 1736.70 | 1736.63 | dry | dry | dry |
| HR-6 | Frozen | Frozen | NM | 1741.31 | 1741.98 | 1741.16 | 1736.50 | 1736.48 | 1738.65 | 1737.11 | 1736.36 |
| HR-7 | 1741.07 | 1740.83 | NM | 1741.36 | 1741.43 | 1741.37 | 1736.89 | 1737.04 | 1736.90 | 1736.89 | 1736.88 |
| HR-8 | 1741.09 | 1740.90 | NM | 1741.42 | 1741.43 | 1741.38 | 1740.07 | 1740.06 | 1739.56 | 1739.55 | 1739.39 |


Groundwater Table Monitoring Elevations in feet

| Well ID | $04 / 13 / 04$ | $05 / 18 / 04$ | $06 / 16 / 04$ | $07 / 15 / 04$ | $08 / 11 / 04$ | $09 / 22 / 04$ | $10 / 09 / 04$ | $11 / 09 / 04$ | $12 / 11 / 04$ | $01 / 18 / 05$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HR-1 | 1740.75 | 1740.22 | 1740.30 | 1740.20 | 1739.89 | 1739.91 | 1739.45 | 1739.89 | 1739.83 | 1739.79 |
| HR-2 | 1741.07 | 1740.20 | 1740.38 | 1740.23 | 1739.84 | 1739.82 | 1739.18 | 1739.77 | 1734.21 | - |
| HR-3 | 1741.05 | 1739.90 | 1739.96 | 1739.92 | 1739.74 | 1739.73 | 1739.28 | 1739.69 | 1739.52 | 1739.57 |
| HR-4 | 1740.63 | 1739.68 | 1739.83 | 1740.03 | 1739.52 | 1739.55 | 1739.23 | 1739.81 | 1735.44 | - |
| HR-5 | 1740.85 | 1739.51 | 1739.53 | 1739.81 | 1739.29 | 1739.32 | 1739.17 | 1739.34 | 1736.72 | 1736.74 |
| HR-6 | 1736.43 | 1736.10 | 1736.33 | 1739.73 | 1736.16 | 1736.16 | 1736.16 | 1736.16 | 1739.97 | 1740.00 |
| HR-7 | 1738.10 | 1737.60 | 1737.51 | 1737.91 | 1737.50 | 1737.52 | 1737.41 | 1737.69 | 1739.92 | 1739.88 |
| HR-8 | 1737.73 | 1737.43 | 1736.78 | 1736.92 | 1737.35 | 1737.44 | 1738.68 | 1737.67 | 1739.98 | 1739.94 |


| MW-1 | 1741.00 | 1739.82 | 1739.89 | 1739.92 | 1739.53 | 1739.45 | 1739.12 | 1739.33 | 1739.75 | 1739.74 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| MW-2 | 1740.59 | 1739.51 | 1739.47 | 1739.82 | 1739.17 | 1739.07 | 1739.10 | 1739.03 | 1737.79 | 1737.77 |
| MW-3 | 1740.12 | 1738.89 | 1738.76 | 1738.92 | 1738.66 | 1738.60 | 1738.76 | 1738.19 | 1739.90 | 1739.85 |
| MW-4 | 1741.36 | 1740.31 | 1740.47 | 1740.25 | 1739.99 | 1739.94 | 1739.56 | 1739.99 | 1739.97 | 1739.91 |
| MW-5 | 1741.22 | 1740.72 | 1740.74 | 1740.59 | 1740.31 | 1740.30 | 1739.94 | 1740.72 | 1738.59 | 1738.59 |
| MW-6 | 1739.83 | 1739.27 | 1742.72 | 1742.44 | 1742.00 | 1741.92 | 1738.06 | 1741.36 | 1738.54 | 1738.60 |
| MW-7 | 1741.45 | 1740.19 | 1740.05 | 1740.02 | 1739.91 | 1739.88 | 1739.51 | 1739.76 | 1740.17 | 1740.10 |
| MW-8 | 1740.76 | 1739.60 | 1739.53 | 1739.73 | 1739.43 | 1739.37 | 1739.18 | 1739.48 | 1740.00 | 1739.44 |
| MW-9 | 1740.94 | 1739.78 | 1739.97 | 1739.96 | 1739.61 | 1739.57 | 1739.12 | 1739.62 | 1739.56 | 1739.54 |
| MW-10 | 1740.90 | 1740.02 | 1740.18 | 1740.06 | 1739.68 | 1739.54 | 1739.50 | 1739.68 | 1737.74 | 1737.68 |
| MW-11 | 1739.96 | 1738.72 | 1738.59 | 1738.95 | NM | 1751.25 | 1738.69 | 1751.25 | 1739.80 | 1739.76 |
| MW-12 | 1740.20 | 1739.72 | 1739.19 | 1739.67 | 1739.83 | 1739.76 | 1739.05 | 1739.96 | 1739.88 | 1739.84 |
| MW-13 | 1738.94 | 1740.06 | 1738.10 | 1739.99 | 1740.38 | 1740.34 | 1739.64 | 1740.23 | 1739.79 | 1739.59 |
| MW-14 | 1739.84 | 1739.76 | 1738.94 | 1740.12 | 1739.42 | 1739.33 | 1739.24 | 1739.38 | 1739.71 | 1739.58 |
| MW-15 | 1740.83 | 1739.72 | 1739.75 | 1739.87 | 1739.43 | 1739.35 | 1738.82 | 1739.22 | 1739.77 | 1739.65 |
| MW-16 | 1740.83 | 1739.99 | 1741.15 | 1740.88 | 1740.19 | 1740.13 | 1739.09 | 1740.06 | 1739.17 | 1738.93 |
| MW-17 | 1739.00 | 1738.82 | 1739.05 | 1738.46 | 1738.35 | 1738.17 | 1737.75 | 1738.13 | 1737.76 | 1737.75 |

Groundwater Table Monitoring
Elevations in feet

| Well ID | $04 / 05 / 05$ | $04 / 19 / 05$ | $05 / 02 / 05$ | $06 / 13 / 05$ | $07 / 11 / 05$ | $08 / 02 / 05$ | $08 / 25 / 05$ | $09 / 13 / 05$ | $11 / 22 / 05$ | $05 / 09 / 06$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HR-1 | 1739.79 | 1739.99 | 1740.10 | 1740.62 | 1740.58 | 1741.63 | 1740.55 | 1741.07 | 1740.02 | 1740.36 |
| HR-2 | 1739.82 | NM | 1733.88 | 1734.28 | 1734.33 | 1741.52 | 1740.73 | 1740.61 | 1734.32 | 1740.45 |
| HR-3 | 1740.27 | NM | 1735.16 | 1735.39 | 1735.47 | 1740.35 | 1740.65 | 1740.40 | 1740.34 | 1740.41 |
| HR-4 | 1739.92 | NM | 1735.04 | 1735.24 | 1735.28 | 1741.08 | 1740.93 | 1740.41 | 1735.21 | 1740.20 |
| HR-5 | 1739.95 | 1739.96 | 1740.02 | 1740.60 | 1740.54 | 1741.20 | 1740.86 | 1740.70 | 1740.70 | 1740.61 |
| HR-6 | 1740.00 | 1740.55 | 1740.64 | 1741.09 | 1741.20 | 1736.08 | 1736.08 | 1736.08 | 1740.54 | 1740.64 |
| HR-7 | 1736.96 | 1737.01 | 1737.36 | 1737.85 | 1737.82 | 1741.10 | 1741.00 | 1739.02 | 1740.55 | 1740.60 |
| HR-8 | 1736.01 | 1736.04 | 1735.02 | 1735.50 | 1735.44 | 1738.15 | 1740.92 | 1738.94 | 1740.58 | 1740.60 |

[^1]APPENDIX D
PNEUMATIC RESPONSE - DATA SUMMARY

VACUUM PRESSURE MONITORING

| Well ID | $\begin{aligned} & 07 / 16 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \text { 07/23/02 } \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 07 / 31 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 08 / 07 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 08 / 15 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 09 / 05 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 09 / 18 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 09 / 23 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline \text { 10/02/02 } \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 10 / 16 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 11 / 18 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 12 / 16 / 02 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 01 / 07 / 03 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HR-1 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0.0 | 5.3 | 1.1 | 0.9 | 0.8 | 1.3 | 0.7 | 0.3 |
| HR-2 | 34.0 | 33.0 | 28.0 | 26.5 | 72.1 | 81.2 | 71.3 | 54.2 | 49.9 | 45.8 | 37.9 | 42.8 | 28.3 |
| HR-3 | 87.0 | 65.0 | 68.0 | 49.5 | 0 | 78.8 | 37.3 | 45.8 | 46.9 | 35.6 | 38.9 | 47.3 | 49.5 |
| HR-4 | 83.0 | 81.0 | 80.0 | 70.0 | 67.5 | 69.8 | 61 | 61.2 | 61.6 | 61.5 | 57.8 | 60.3 | 63.2 |
| HR-5 | 102.0 | 98.0 | 87.0 | 90.0 | 101.5 | 83.5 | 80.2 | 81.6 | 80.4 | 84.5 | 84.2 | 85.5 | 86.1 |
| HR-6 | 0.0 | 5.8 | 4.7 | 4.5 | 7 | 9.6 | 5.5 | 7.7 | 7.7 | 8.1 | 7.4 | 5.9 | 5.4 |
| HR-7 | 0.0 | 1.3 | 1.1 | 1.2 | 1.3 | 1.3 | 1.4 | 1.1 | 1.4 | 1.3 | 1.1 | 0.8 | 0.7 |
| HR-8 | 0.0 | 1.7 | 1.2 | 1.4 | 1.5 | 1.5 | 1.4 | 1.1 | 1.2 | 1.3 | 1.1 | 0.7 | 0.7 |
| MW-1 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0.0 | 0.2 | 0 | 0 | 0.8 | 0.3 | 0.2 | 0.2 |
| MW-2 | 20.0 | 24.2 | 23.8 | 26.8 | 26.8 | 32.1 | 31.7 | 31.3 | 30.4 | 34.4 | 29.2 | 29.6 | 29.2 |
| MW-3 | 0.0 | 1.2 | 0.9 | 1.0 | 1.2 | 1.1 | 1.2 | 1 | 0.9 | 1.1 | 0.9 | 0.7 | 0.7 |
| MW-10 | 12.8 | 11.0 | 11.1 | 8.5 | 24 | 22.1 | 26.2 | 16.4 | 16.4 | 11.9 | 7.8 | 16.1 | 11.8 |
| MW-11 | 0.0 | 0.0 | 0.0 | 0.8 | 1.2 | 1.1 | 1.1 | 0.9 | 0.9 | 1.1 | 0.8 | 0.6 | 0.5 |
| MW-12 | 0.0 | 0.0 | 0.0 | 1.3 | 1.7 | 0.3 | 0.2 | 3.1 | 3.1 | 2.6 | 4.7 | 0.8 | 0.9 |
| MW-13 | 0.0 | 8.5 | 9.5 | 8.8 | 10.5 | 10.7 | 9.3 | 8.5 | 8.5 | 8.9 | 8.2 | 6.8 | 6.1 |
| MW-14 | 0.0 | 5.7 | 2.5 | 2.2 | 5.9 | 4.6 | 7.8 | 7.8 | 7.8 | 9.2 | 10.2 | 8.7 | 7.5 |
| MW-15 | 3.5 | 3.6 | 3.3 | 3.7 | 3.4 | 4.2 | 1.2 | 3.3 | 3.3 | 5.4 | 4.3 |  | 4.6 |

[^2]VACUUM PRESSURE MONITORING (Continued)

| Well ID | $\begin{aligned} & 04 / 13 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 05 / 18 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 06 / 16 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 07 / 15 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 08 / 11 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 09 / 22 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 10 / 09 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 11 / 09 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & 12 / 11 / 04 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \end{aligned}$ | $\begin{aligned} & \hline 01 / 18 / 05 \\ & \text { (in. } \mathrm{H}_{2} \mathrm{O} \text { ) } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HR-1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| HR-2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42.6 | 40.1 |
| HR-3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| HR-4 | 5.5 | 0 | 5.9 | 0 | 4.1 | 3.7 | 1.4 | 2.9 | 66.1 | 69.3 |
| HR-5 | 3.7 | 0 | 4.3 | 0 | 2.9 | 2.6 | 1.3 | 1.7 | 88 | 67.7 |
| HR-6 | 94.4 | 100.1 | 163.2 | 123.8 | 98.1 | 89.9 | 51.2 | 78.3 | 0 | 0 |
| HR-7 | 10.1 | 20.6 | 18.3 | 15.8 | 22.3 | 20.4 | 19.3 | 19.3 | 0.7 | 0.5 |
| HR-8 | 85.1 | 105.6 | 20.6 | 17.7 | 16.9 | 15.8 | 11.3 | 14.6 | 0.5 | 0.2 |
| MW-1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MW-2 | 5.4 | 0 | 4.4 | 0 | 3.9 | 2.8 | 1.3 | 1.5 | 47 | 45.5 |
| MW-3 | 6.1 | 8.4 | 17.7 | 6.9 | 7.3 | 6.9 | 6.1 | 3.6 | 0 | 0 |
| MW-10 | 0 | 0 | 2.6 | 0 | 0 | 0 | 0 | 0 | 3 | 2.6 |
| MW-11 | 7.6 | 9.5 | 19.4 | 6.1 | 7.3 | 6.3 | 6.3 | 5.7 | 0.5 | 0.3 |
| MW-12 | 0.3 | 11.5 | 30.6 | 12.5 | 13.2 | 12.9 | 8.1 | 11.1 | 1.4 | 1.2 |
| MW-13 | 33.3 | 36.1 | 58.7 | 0 | 38.2 | 37.1 | 15.7 | 28.2 | 3 | 2.1 |
| MW-14 | 19.7 | 18.4 | 34.6 | 0 | 16 | 15.6 | 6.4 | 13.3 | 6.3 | 5.9 |
| MW-15 | 0.3 | 0 | 72.4 | 0 | 1 | 0.5 | 0.5 |  | 2.8 | 2.2 |



## APPENDIX E

## MASS BALANCE WORKSHEETS

## APPENDIX E-1

## CONTAMINANT RECOVERY - LIQUID PHASE

Contaminant Recovery - Liquid Phase

| Date | Totalizer (gal) | Flow (gpm) | $\begin{gathered} \mathrm{TPH}_{\text {water }} \\ \mathrm{mg} / \mathrm{l} \end{gathered}$ | BTEX <br> mg/l | TPH Mass <br> (lb) | BTEX Mass <br> (Ib) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Well field HR-2, 3, 4, 5 |  |  |  |  |  |  |
| 07/11/02 | 0 |  | 74.3 | 32.7 |  |  |
| 07/16/02 | 45,100 | 10.5 | 57.0 | 22.2 | 24.7 | 10.3 |
| 07/23/02 | 49,908 | 9.9 | 51.5 | 20.3 | 2.2 | 0.9 |
| 08/15/02 | 177,277 | 9.9 | 68.8 | 28.5 | 63.9 | 25.9 |
| 09/18/02 | 267,961 | 10.5 | 35.2 | 15.1 | 39.3 | 16.5 |
| 09/24/02 | 340,139 | 8.0 | 67.7 | 22.6 | 31.0 | 11.4 |
| 10/02/02 | 403,460 | 5.6 | 44.1 | 16.6 | 29.5 | 10.4 |
| 10/16/02 | 509,217 | 5.2 | 30.7 | 11.1 | 33.0 | 12.2 |
| 11/18/02 | 750,129 | 6.0 | 20.7 | 6.0 | 51.7 | 17.2 |
| 12/16/02 | 909,574 | 4.0 | 15.3 | 5.7 | 23.9 | 7.8 |
| 01/07/03 | 1,027,069 | 3.7 | 12.6 | 4.93 | 13.8 | 5.2 |
| Well field HR-1, 2, 3, 4, 5 |  |  |  |  |  |  |
| 03/28/03 | 1,034,482 | 5.7 | 53.4 | 16.48 | 2.9 | 0.9 |
| 04/23/03 | 1,196,925 | 4.3 | 16.2 | 7.34 | 47.2 | 16.1 |
| 05/19/03 | 1,378,891 | 4.8 | 14.8 | 6.05 | 23.5 | 10.2 |
| Well field HR-2, 3, 4, 5 |  |  |  |  |  |  |
| 06/17/03 | 1,665,824 | 6.9 | 4.9 | 2.15 | 23.6 | 9.8 |
| 07/15/03 | 1,796,418 | 4.3 | 3.4 | 1.85 | 4.5 | 2.2 |
| Well field HR-4, 5, 6, 7 |  |  |  |  |  |  |
| 07/22/03 | 1,847,512 | 5.2 | 15 | 8.80 | 1.4 | 0.8 |
| 08/21/03 | 2,230,972 | 10.4 | 20 | 8.80 | 56.0 | 28.2 |
| 09/23/03 | 2,551,793 | 10.4 | 15.1 | 7.83 | 47.0 | 22.3 |
| 10/22/03 | 2,829,793 | 8.4 | 9.7 | 3.97 | 28.8 | 13.7 |
| 11/17/03 | 3,144,793 | 8.5 | 10 | 2.90 | 25.9 | 9.0 |
| 12/17/03 | 3,503,086 | 8.5 | 4.9 | 1.96 | 22.3 | 7.3 |
| 01/05/04 | 3,682,286 | 7.1 | 4.9 | 1.96 | 7.9 | 3.2 |
| Well fields HR-4, 5, 6, 7 and HR-6, 7, 8 |  |  |  |  |  |  |
| 04/13/04 | 3,711,086 | 10.0 | 6.2 | 1.85 | 0.7 | 0.2 |
| 05/18/04 | 4,235,969 | 11.4 | 5.1 | 1.82 | 24.7 | 8.0 |
| 06/16/04 | 4,694,156 | 11.0 | 4.3 | 1.69 | 18.0 | 6.7 |
| 07/15/04 | 5,133,582 | 10.7 | 8.0 | 3.10 | 22.6 | 8.8 |
| 08/10/04 | 5,396,932 | 8.9 | 4.7 | 1.55 | 14.0 | 5.1 |
| 09/22/04 | 5,702,666 | 8.2 | 4.0 | 0.93 | 11.2 | 3.2 |
| 10/16/04 | 5,896,606 | 5.8 | 2.0 | 0.45 | 4.9 | 1.1 |
| 11/09/04 | 6,086,103 | 5.8 | 2.0 | 0.03 | 3.2 | 0.4 |
| Well field 2, 4, 5 |  |  |  |  |  |  |
| 11/09/04 | 6,086,103 |  | 189.0 | 40.10 |  |  |
| 12/15/04 | 6,105,708 | 0.4 | 9.0 | 2.50 | 16.2 | 3.5 |
| 01/18/05 | 6,131,792 | 0.5 | 2.8 | 0.69 | 1.3 | 0.3 |
| Well field 2, 3, 4 |  |  |  |  |  |  |
| 04/06/05 | 6,131,792 | 0.0 | 9.0 | 4.48 | 0.0 | 0.0 |
| 04/19/05 | 6,153,892 | 1.1 | 5.2 | 2.24 | 1.3 | 0.6 |
| 05/02/05 | 6,171,278 | 0.9 | 3.2 | 1.27 | 0.6 | 0.3 |
| 06/13/05 | 6,271,395 | 1.7 | 0.1 | 0.43 | 1.4 | 0.7 |
| Well field 6, 7, 8 |  |  |  |  |  |  |
| 07/11/05 | 6,375,720 | 2.6 | 1.0 | 0.58 | 0.5 | 0.4 |
| 08/02/05 | 6,440,365 | 2.1 | 0.1 | 0.00 | 0.3 | 0.2 |
| 08/25/05 | 6,506,493 | 2.0 | 0.4 | 0.03 | 0.1 | 0.0 |
| 09/13/05 | 6,625,569 | 4.4 | 0.1 | 0.02 | 0.3 | 0.0 |
| Well field 2, 4, 5 |  |  |  |  |  |  |
| 10/13/05 | 6631673 | 1.2 | 0.2 | 0.02 | 0.0 | 0.0 |
| 11/22/05 | 6707299 | 1.3 | 0.0 | 0.02 | 0.1 | 0.0 |
| Total | 6,707,299 |  |  |  | 725.3 | 281.0 |

## APPENDIX E-2

## CONTAMINANT RECOVERY - VAPOR PHASE

Contaminant Recovery TPH - Vapor Phase

| Date | Runtime (hours) | $\begin{aligned} & \mathbf{Q}_{\text {air }} \\ & (\mathrm{cfm}) \end{aligned}$ | Volume $\left(1000 \mathrm{ft}^{3}\right)$ | $\begin{aligned} & \mathrm{TPH}_{\mathrm{air}}{ }^{1} \\ & \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{aligned}$ | $\begin{aligned} & \text { BTEX }_{\text {air }}{ }^{1} \\ & \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{aligned}$ | TPH Mass <br> (Ib) | BTEX Mass <br> (lb) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Well field HR-2, 3, 4, 5 |  |  |  |  |  |  |  |
| 07/11/02 | 4 | 80 | 19 | 218,000 | 6,440 |  |  |
| 07/16/02 | 72 | 100 | 432 | 73,500 | 2,431 | 2953 | 92 |
| 09/18/02 | 367 | 100 | 2,202 | 98,300 | 5,213 | 11807 | 525 |
| 09/24/02 | 150 | 126 | 1,134 | 58,900 | 3,056 | 5566 | 293 |
| 10/02/02 | 189 | 124 | 1,406 | 43,050 | 1,712 | 4475 | 209 |
| 10/16/02 | 336 | 126 | 2,541 | 19,850 | 646 | 4990 | 187 |
| 11/18/02 | 666 | 127 | 5,074 | 9,125 | 419 | 4589 | 169 |
| 12/16/02 | 666 | 133 | 5,299 | 8,495 | 299 | 2914 | 119 |
| 01/07/03 | 529 | 126 | 3,998 | 6,325 | 284 | 1847 | 72 |
| Well field HR-1, 2, 3, 4, 5 |  |  |  |  |  |  |  |
| 03/28/03 | 19 | 132 | 149 | 51,450 | 638 | 477 | 6 |
| 04/23/03 | 623 | 153 | 5,723 | 8,455 | 384 | 6861 | 160 |
| 05/19/03 | 629 | 122 | 4,603 | 4,155 | 155 | 1812 | 77 |
| Well field HR-2, 3, 4, 5 |  |  |  |  |  |  |  |
| 06/17/03 | 695 | 83 | 3,463 | 2620 | 182 | 732 | 36 |
| 07/15/03 | 512 | 101 | 3,105 | 2160 | 114 | 463 | 29 |
| 07/22/03 | 164 | 50 | 995 | 2160 | 114 | 134 | 7 |
| 07/22/03 | Well field HR-4, 5, 6, 7 |  |  | 6995 | 132 |  |  |
| 08/21/03 | 616 | 74 | 2,736 | 11200 | 401 | 1734 | 57 |
| 09/23/03 | 513 | 58 | 1,786 | 13100 | 687 | 1354 | 61 |
| 10/22/03 | 550 | 81 | 2,672 | 5155 | 289 | 1522 | 81 |
| 11/17/03 | 616 | 123 | 4,550 | 508 | 56 | 804 | 49 |
| 12/17/03 | 702 | 95 | 4,001 | 1090 | 10 | 200 | 8 |
| 01/05/04 | 456 | 95 | 2,594 | 1090 | 0 | 176 | 1 |
|  | Well field 4, 5, 6, 7 and 6, 7, 8 |  |  |  | 0 |  | 0 |
| 04/13/04 |  |  |  | 10355 | 62 | 68 | 10 |
| 05/18/04 | 768 | 75 | 3,456 | 1680 | 30 | 830 | 8 |
| 06/16/04 | 696 | 78 | 3,257 | 1325 | 48 | 306 | 26 |
| 07/15/04 | 686 | 85 | 3,499 | 20200 | 191 | 2351 | 16 |
| 08/10/04 | 492 | 79 | 2,332 | 1645 | 25 | 1590 | 4 |
| 09/22/04 | 624 | 72 | 2,696 | 392 | 21 | 171 | 10 |
| 10/16/04 | 560 | 86 | 2,890 | 1760 | 86 | 194 | 7 |
| 11/09/04 | 542 | 83 | 2,699 | 0 | 1 | 148 | 0 |
|  | Well field 2, 4, 5 |  |  |  |  |  |  |
| 11/09/04 | 0 | 83 | 0 | 2860 | 146 | 0 | 45 |
| 12/15/04 | 792 | 79 | 3,754 | 1720 | 240 | 537 | 31 |
| 01/18/05 | 808 | 82 | 3,975 | 0 | 6 | 213 | 1 |
|  | Well field 2, 3, 4 |  |  |  |  |  |  |
| 04/06/05 | 19 | 95 | 105 | 4535 | 343 | 30 | 24 |
| 04/19/05 | 304 | 83 | 1,514 | 1345 | 160 | 278 | 11 |
| 05/02/05 | 312 | 84 | 1,572 | 845 | 61 | 107 | 32 |
| 06/13/05 | 1008 | 80 | 4,838 | 727 | 148 | 237 | 24 |
| 07/11/05 | 670 | 84 | 3,377 | 326 | 75 | 111 | 0 |
|  | Well field 6, 7, 8 |  |  |  |  |  |  |
| 07/11/05 |  | - | 0 | 0 | 0 | 0 | 0 |
| 08/02/05 | 520 | 84 | 2,621 | 0 | 0 | 0 | 0 |
| 08/25/05 | 550 | 82 | 2,706 | 0 | 0 | 0 | 0 |
| 09/13/05 | 453 | 78 | 2,120 | 0 | 0 | 0 | 0 |
| 09/14/05 | 21 | 78 | 98 | 0 | 3 | 0 | 0 |
|  | Well field 2, 4, 5 |  |  |  |  |  |  |
| 10/13/05 | 6 | 51 | 18 | 0 | 21 | 0 | 0.0 |
| 11/22/05 | 960 | 82 | 4,723 | 0 | 0 | 0 | 3.1 |
| Total | 19,889 |  | 110,838 |  |  | 62,584 | 2,490 |

## APPENDIX F

## SUMMARY OF ANALYTICAL DATA GROUNDWATER QUALITY MONITORING

APPENDIX F-1

## COC IN GROUNDWATER

Groundwater Quality Monitoring - MBTEX Scan

| Well ID | Date | $\begin{gathered} \hline \text { MTBE } \\ \mathrm{ppb} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Benzene } \\ \text { ppb } \end{gathered}$ | $\begin{gathered} \text { Toluene } \\ \text { ppb } \end{gathered}$ | Ethylbenz. ppb | Xylenes (total) ppb | GRO (TPH) mg/l | $\begin{gathered} \text { BTEX } \\ \mathrm{ppb} \end{gathered}$ | $\begin{aligned} & \text { BTEX } \\ & \text { Trend } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MW-1 | 04/08/02 | <250 | 34000 | 7790 | 2200 | 6440 | 133.0 | 50430 |  |
| MW-1 | 11/19/02 | <200 | 19000 | 5030 | 1680 | 2650 | 89.4 | 28360 |  |
| MW-1 | 04/23/03 | <200 | 15400 | 6250 | 1680 | 2920 | 65.2 | 26250 |  |
| MW-1 | 11/17/03 | <250 | 9816 | 1505 | 1960 | 3246 | 63.1 | 16527 |  |
| MW-1 | 05/18/04 | <100 | 5849 | 401.8 | 1409 | 1688 | 29.9 | 9348 | $\nabla$ |
| MW-1 | 10/09/04 | <100 | 7817 | 4808 | 2113 | 6488 | 46.7 | 21226 |  |
| MW-1 | 05/04/05 | 364.2 | 4933 | 1088 | 1991 | 4361 | 37.1 | 12373 |  |
| MW-1 | 11/22/05 | <50 | 1449 | <50 | 1369 | 909.9 | 18.15 | 3728 |  |
| MW-1 | 05/09/06 | <50 | 978 | 56.6 | 1284 | 1194 | 16.20 | 3513 |  |
| MW-2 | 04/09/02 | <20 | 4010 | 326 | 305 | 752 | 16.3 | 5393 |  |
| MW-2 | 11/19/02 | <5 | 343 | <5 | 14.3 | <15 | 2.2 | 357 |  |
| MW-2 | 04/23/03 | <5 | 686 | 22.2 | 6.7 | <15 | 2.4 | 715 |  |
| MW-2 | 11/17/03 | <1 | 91 | 10.2 | 7.3 | 12.8 | 0.9 | 121 |  |
| MW-2 | 05/18/04 | <5 | 996 | 19.1 | 18 | 17.8 | 2.2 | 1051 | $\nabla$ |
| MW-2 | 10/09/04 | <5 | 1328 | 5.3 | 342.5 | 25.1 | 4.5 | 1701 |  |
| MW-2 | 05/04/05 | <1 | 3.4 | 2.2 | 1.8 | <3 | 0.3 | 7 |  |
| MW-2 | 11/22/05 | <1 | 2.1 | <1 | <1 | $<3$ | <0.2 | 2 |  |
| MW-2 | 05/09/06 | <1 | 12.5 | $<1$ | 3.4 | 5.7 | <0.2 | 22 |  |
| MW-3 | 04/09/02 | <20 | 777 | 1240 | 77.3 | 636 | 7.3 | 2730 |  |
| MW-3 | 11/19/02 | <10 | 214 | 969 | 46.9 | 648 | 4.9 | 1878 |  |
| MW-3 | 04/23/03 | <10 | 236 | 1630 | 82.1 | 1900 | 8.0 | 3848 |  |
| MW-3 | 11/17/03 | <1 | 1.6 | <1 | 5.7 | 37.1 | 0.6 | 44 |  |
| MW-3 | 05/18/04 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 | $\nabla$ |
| MW-3 | 10/09/04 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-3 | 05/04/05 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-3 | 11/22/05 | <1 | 1.1 | <1 | <1 | <3 | <0.2 | , |  |
| MW-3 | 05/09/06 | $<1$ | <1 | <1 | $<1$ | $<3$ | <0.2 | 0 |  |
| MW-4 | 04/08/02 | <1 | <1 | <1 | <1 | $<3$ | <0.2 | 0 |  |
| MW-4 | 11/19/02 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-4 | 04/23/03 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-4 | 11/17/03 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-4 | 05/18/04 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 | - |
| MW-4 | 10/09/04 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-4 | 05/04/05 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-4 | 11/22/05 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-4 | 05/09/06 | <1 | $<1$ | <1 | <1 | $<3$ | <0.2 | 0 |  |
| MW-5 | 04/08/02 | <200 | 30000 | 4000 | 584 | 977 | 101.0 | 35561 |  |
| MW-5 | 11/19/02 | <500 | 29000 | 15300 | 1070 | 2930 | 109.0 | 48300 |  |
| MW-5 | 04/23/03 | <500 | 19800 | 20800 | 1620 | 4430 | <100 | 46650 |  |
| MW-5 | 11/17/03 | <500 | 13900 | 10930 | 2073 | 5122 | 76.2 | 32025 |  |
| MW-5 | 05/18/04 | <50 | 3502 | 1439 | 709.5 | 1476 | 18.7 | 7127 | $\nabla$ |
| MW-5 | 10/09/04 | <100 | 7706 | 10370 | 2730 | 6766 | 61.1 | 27572 |  |
| MW-5 | 05/04/05 | 89.7 | 497.3 | 274.6 | 248.1 | 587.5 | 5.3 | 1608 |  |
| MW-5 | 11/22/05 | <10 | 1455 | 742 | 1804 | 2147 | 24.0 | 6148 |  |
| MW-5 | 05/09/06 | <20 | 4754 | 1817 | 2417 | 2807 | 31.32 | 11795 |  |
| MW-6 | 04/08/02 | <100 | 11100 | <100 | 213 | <300 | 28.0 | 11313 |  |
| MW-6 | 11/19/02 | <50 | 5380 | <50 | 119 | <150 | 13.5 | 5499 |  |
| MW-6 | 04/23/03 | <50 | 6150 | <50 | 152 | <150 | 13.9 | 6302 |  |
| MW-6 | 11/17/03 | <100 | 10880 | <100 | 392.5 | <300 | 27.5 | 11273 |  |
| MW-6 | 05/18/04 | 54.6 | 7638 | <50 | 269.4 | <150 | 15.8 | 7907 | $\nabla$ |
| MW-6 | 10/09/04 | <50 | 4460 | <50 | 208.9 | <150 | 11.2 | 4669 |  |
| MW-6 | 05/04/05 | <50 | 793.9 | <50 | 80.5 | <150 | 3.0 | 874 |  |
| MW-6 | 11/22/05 | <20 | 397.4 | 31.5 | 101.8 | <60 | 2.440 | 531 |  |
| MW-6 | 05/09/06 | <1 | 209.5 | 1.6 | 58 | 3,6 | 1.52 | 269 |  |


| Well ID | Date | $\begin{gathered} \hline \text { MTBE } \\ \mathrm{ppb} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Benzene } \\ \mathrm{ppb} \end{gathered}$ | $\begin{gathered} \hline \text { Toluene } \\ \text { ppb } \end{gathered}$ | Ethylbenz. ppb | Xylenes (total) ppb | $\begin{gathered} \hline \text { GRO (TPH) } \\ \mathrm{mg} / \mathrm{l} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { BTEX } \\ \mathrm{ppb} \\ \hline \end{gathered}$ | BTEX Trend |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MW-7 | 04/08/02 | <1 | <1 | <1 | <1 | $<3$ | <0.2 | 0 |  |
| MW-7 | 11/19/02 | <1 | <1 | <1 | <1 | $<3$ | <0.2 | 0 |  |
| MW-7 | 04/23/03 | <1 | <1 | <1 | <1 | $<3$ | <0.2 | 0 |  |
| MW-7 | 11/17/03 | <1 | <1 | <1 | <1 | $<3$ | <0.2 | 0 |  |
| MW-7 | 05/18/04 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 | - |
| MW-7 | 10/09/04 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-7 | 05/04/05 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-7 | 11/22/05 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-7 | 05/09/06 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-8 | 04/08/02 | <1 | <1 | $<1$ | <1 | $<3$ | <0.2 | 0 |  |
| MW-8 | 11/19/02 | <1 | <1 | 1.2 | <1 | $<3$ | <0.2 | 1 |  |
| MW-8 | 04/23/03 | <1 | 6.8 | 5.2 | <1 | <3 | <0.2 | 12 |  |
| MW-8 | 05/15/03 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-8 | 11/17/03 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-8 | 05/18/04 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-8 | 10/09/04 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-8 | 05/04/05 | <1 | <1 | <1 | <1 | $<3$ | 0.2 | 0 |  |
| MW-8 | 11/22/05 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-8 | 05/09/06 | $<1$ | $<1$ | $<1$ | <1 | $<3$ | <0.2 | 0 |  |
| MW-9 | 04/08/02 | <1 | <1 | $<1$ | <1 | <3 | <0.2 | 0 |  |
| MW-9 | 11/19/02 | <1 | <1 | 1.5 | <1 | $<3$ | <0.2 | 2 |  |
| MW-9 | 04/23/03 | <1 | 1.3 | 1.8 | <1 | <3 | <0.2 | 3 |  |
| MW-9 | 05/15/03 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-9 | 11/17/03 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-9 | 05/18/04 | <1 | <1 | <1 | <1 | $<3$ | <0.2 | 0 |  |
| MW-9 | 10/09/04 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-9 | 05/04/05 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-9 | 11/22/05 | <1 | <1 | 1.1 | <1 | <3 | <0.2 | 1 |  |
| MW-9 | 05/09/06 | $<1$ | $<1$ | $<1$ | $<1$ | $<3$ | <0.2 | 0 |  |
| MW-10 | 04/08/02 | $<500$ | 52800 | 16600 | 1470 | 4160 | 167.0 | 75030 |  |
| MW-10 | 11/19/02 | <200 | 20600 | 419 | 532 | <600 | 40.1 | 21551 |  |
| MW-10 | 04/23/03 | <200 | 19900 | 3480 | 1160 | 3790 | 59.2 | 28330 |  |
| MW-10 | 11/17/03 | <500 | 6722 | 1032 | 1058 | 3476 | 29.3 | 12288 |  |
| MW-10 | 05/18/04 | <50 | 5439 | 108.4 | 772.2 | 2598 | 24.4 | 8918 | $\nabla$ |
| MW-10 | 10/09/04 | <100 | 24810 | 46110 | 5857 | 24800 | 209.1 | 101577 |  |
| MW-10 | 05/04/05 | <200 | 6430 | 12290 | 2859 | 15570 | 100.8 | 37149 |  |
| MW-10 | 11/22/05 | <200 | 5269 | 8342 | 1787 | 7124 | 54.76 | 22522 |  |
| MW-10 | 05/09/06 | <200 | 5696 | 13940 | 2850 | 13360 | 71.91 | 35846 |  |
| MW-11 | 07/23/02 | <200 | 5310 | 14100 | 1920 | 12500 | 107.0 | 33830 |  |
| MW-11 | 11/19/02 | <500 | 8160 | 40200 | 3830 | 19800 | 170.0 | 71990 |  |
| MW-11 | 04/23/03 | <100 | 1780 | 5110 | 662 | 6970 | 40.5 | 14522 |  |
| MW-11 | 11/17/03 | <10 | 30.5 | 11.5 | 75.7 | 356 | 5.0 | 474 |  |
| MW-11 | 05/18/04 | <5 | 11.2 | <5 | 5.5 | 136.6 | 3.3 | 153 | $\nabla$ |
| MW-11 | 10/09/04 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-11 | 05/04/05 | <1 | <1 | <1 | <1 | <3 | 0.2 | 0 |  |
| MW-11 | 11/22/05 | <1 | <1 | <1 | <1 | <3 | <0.2 | 0 |  |
| MW-11 | 05/09/06 | $<1$ | $<1$ | $<1$ | $<1$ | $<3$ | <0.2 | 0 |  |
| MW-12 | 07/23/02 | <100 | 34700 | 29200 | 2180 | 9940 | 163.0 | 76020 |  |
| MW-12 | 11/19/02 | <200 | 40600 | 21000 | 2130 | 7370 | 159.0 | 71100 |  |
| MW-12 | 04/23/03 | <200 | 37700 | 13000 | 2140 | 5370 | 123.0 | 58210 |  |
| MW-12 | 11/17/03 | <500 | 35610 | 13150 | 1524 | 6506 | 148.6 | 56790 |  |
| MW-12 | 05/18/04 | <20 | 1347 | 147.4 | 170.9 | 576.9 | 6.1 | 2242 | - |
| MW-12 | 10/09/04 | $<20$ | 3368 | 87.6 | 194.9 | 1361 | 13.8 | 5012 |  |
| MW-12 | 05/04/05 | 58.5 | 1384 | 174.9 | 70.8 | 209.9 | 5.2 | 1840 |  |
| MW-12 | 11/22/05 | <50 | 15990 | 4005 | 519.3 | 1561 | 46.4 | 22075 |  |
| MW-12 | 05/09/06 | <100 | 36750 | 19340 | 1426 | 7937 | 100.8 | 65453 |  |


| Well ID | Date | MTBE ppb | Benzene ppb | Toluene ppb | Ethylbenz. ppb | Xylenes (total) ppb | GRO (TPH) mg/l | $\begin{gathered} \text { BTEX } \\ \text { ppb } \end{gathered}$ | BTEX <br> Trend |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MW-13 | 07/10/02 | <1000 | 47900 | 21900 | 2590 | 9970 | 201.0 | 82360 |  |
| MW-13 | 11/19/02 | <200 | 33600 | 15500 | 2130 | 7190 | 148.0 | 58420 |  |
| MW-13 | 04/23/03 | <200 | 36400 | 18500 | 2290 | 8400 | 137.0 | 65590 |  |
| MW-13 | 11/17/03 | <100 | 4020 | 1153 | 430.7 | 1530 | 20.9 | 7134 |  |
| MW-13 | 05/18/04 | <50 | 2519 | 1126 | 278.4 | 827.8 | 10.3 | 4751 | $\nabla$ |
| MW-13 | 10/09/04 | <5 | 308.6 | <5 | 43.2 | <15 | 1.4 | 352 |  |
| MW-13 | 05/04/05 | 29.4 | 211.9 | 7.6 | 118.9 | 37.2 | 2.82 | 376 |  |
| MW-13 | 11/22/05 | <5 | 62.5 | <5 | 85.8 | 17.9 | 1.552 | 166 |  |
| MW-13 | 05/09/06 | <2 | 37.7 | <2 | 117.9 | 24.5 | 1.824 | 180 |  |
| MW-14 | 07/23/02 | <200 | 34400 | 36300 | 3260 | 17100 | 209.0 | 91060 |  |
| MW-14 | 11/19/02 | <500 | 36300 | 24600 | 2340 | 9640 | 161.0 | 72880 |  |
| MW-14 | 04/23/03 | <500 | 30400 | 24200 | 2480 | 10900 | 140.0 | 67980 |  |
| MW-14 | 11/17/03 | <500 | 27990 | 15060 | 2187 | 7560 | 118.0 | 52797 |  |
| MW-14 | 05/18/04 | <200 | 13800 | 3714 | 1502 | 6266 | 54.9 | 25282 | $\nabla$ |
| MW-14 | 10/09/04 | <200 | 9230 | 2196 | 1184 | 2259 | 29.9 | 14869 |  |
| MW-14 | 05/04/05 | <100 | 2153 | <100 | 628.4 | 682.8 | 13.44 | 3464 |  |
| MW-14 | 11/22/05 | <20 | 544.3 | 14.9 | 241.8 | 223 | 14.79 | 1024 |  |
| MW-14 | 05/09/06 | <10 | 2441 | 21.7 | 777.2 | 274.8 | 10.68 | 3515 |  |
| MW-15 | 07/23/02 | <500 | 31900 | 27700 | 2610 | 10700 | 174.0 | 72910 |  |
| MW-15 | 11/19/02 | <200 | 22000 | 11700 | 1840 | 5490 | 95.8 | 41030 |  |
| MW-15 | 04/23/03 | <200 | 26100 | 13000 | 2190 | 7200 | 97.6 | 48490 |  |
| MW-15 | 11/17/03 | <500 | 10830 | 32560 | 7169 | 29440 | 177.0 | 79999 |  |
| MW-15 | 05/18/04 | <200 | 14380 | 2759 | 2391 | 6573 | 62.1 | 26103 | $\nabla$ |
| MW-15 | 10/09/04 | <200 | 10050 | 30250 | 13650 | 27630 | 208.5 | 81580 |  |
| MW-15 | 05/04/05 | <200 | 7151 | 13810 | 2779 | 14610 | 90.4 | 38350 |  |
| MW-15 | 11/22/05 | <200 | 841 | 1972 | 1397 | 9100 | 42.33 | 13310 |  |
| MW-15 | 05/09/06 | <50 | 844 | 1692 | 1516 | 7963 | 29.55 | 12015 |  |
| MW-16 | 07/10/02 | <250 | 26400 | <250 | 304 | <750 | 52.1 | 26704 |  |
| MW-16 | 11/19/02 | <100 | 28300 | <100 | 437 | <300 | 61.1 | 28737 |  |
| MW-16 | 04/23/03 | <100 | 23100 | <100 | 199 | <300 | 47.5 | 23299 |  |
| MW-16 | 11/17/03 | <500 | 37290 | <500 | 1378 | <1500 | 104.0 | 38668 |  |
| MW-16 | 05/18/04 | <100 | 31920 | 139.5 | 1006 | <300 | 53.6 | 33066 | $\nabla$ |
| MW-16 | 10/09/04 | <100 | 31000 | <100 | 1773 | <300 | 61.4 | 32773 |  |
| MW-16 | 05/04/05 | <500 | 24070 | <500 | 1315 | <1500 | 48.23 | 25385 |  |
| MW-16 | 11/22/05 | <250 | 22370 | <250 | 1942 | <750 | 56.02 | 24312 |  |
| MW-16 | 05/09/06 | $<50$ | 19130 | 133.6 | 1233 | 177.4 | 34.16 | 20674 |  |
| MW-17 | 07/10/02 | <1 | 11.9 | 3 | <1 | <3 | <0.2 | 15 |  |
| MW-17 | 11/19/02 | $<1$ | <1 | $<1$ | $<1$ | <3 | <0.2 | 0 |  |
| MW-17 | 04/23/03 | $<1$ | $<1$ | $<1$ | <1 | $<3$ | <0.2 | 0 |  |
| MW-17 | 11/17/03 | $<1$ | $<1$ | $<1$ | $<1$ | $<3$ | <0.2 | 0 |  |
| MW-17 | 05/18/04 | $<1$ | $<1$ | $<1$ | $<1$ | <3 | <0.2 | 0 | - |
| MW-17 | 10/09/04 | <1 | 13 | $<1$ | <1 | $<3$ | 0.2 | 13 |  |
| MW-17 | 05/04/05 | $<1$ | <1 | $<1$ | $<1$ | $<3$ | $<0.2$ | 0 |  |
| MW-17 | 11/22/05 | $<1$ | 11.2 | <1 | $<1$ | $<3$ | <0.2 | 11 |  |
| MW-17 | 05/09/06 | <1 | <1 | <1 | <1 | $<3$ | <0.2 | 0 |  |

## APPENDIX F-2

## BIODEGRADATION INDICATORS

Groundwater Quality Monitoring - Selected Biodegradation Parameters

|  |  | MW-1 | MW-1 | MW-1 | MW-1 | MW-1 | MW-1 | MW-1 | MW-1 | MW-1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Units | $07 / 10 / 02$ | $11 / 19 / 02$ | $04 / 23 / 03$ | $11 / 17 / 03$ | $05 / 18 / 04$ | $10 / 9 / 04$ | $5 / 4 / 05$ | $11 / 22 / 05$ | $5 / 9 / 06$ |
| Sulfate | $\mathrm{mg} / \mathrm{I}$ | 12.6 | 6.4 | 37.9 | 33.6 | 288 | 66.2 | 42.4 | 56.9 | 47.7 |
| Nitrate-Nitrite as N | $\mathrm{mg} / \mathrm{l}$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| BOD | $\mathrm{mg} / \mathrm{l}$ | 0.11 | 106 | 103 | 79.8 | 56.2 | 126 | 32.6 | 16.3 | $<20$ |
| Fe (total) | $\mathrm{mg} / \mathrm{l}$ | 10.4 | 27.3 | 41.8 | 25.4 | 14.4 | 27.2 | 22.9 | 4.46 | 5.86 |
| Fe (dissolved) | $\mathrm{mg} / \mathrm{l}$ | 4.5 | 2.21 | 3.58 | 2.04 | 2.24 | 1.14 | 0.57 | 3.03 | 3.16 |
| Mn (total) | $\mathrm{mg} / \mathrm{l}$ | 1.95 | 2.41 | 2.99 | 2.12 | 2.95 | 2.3 | 2.34 | 1.57 | 1.38 |
| Mn (dissolved) | $\mathrm{mg} / \mathrm{l}$ | 1.69 | 2.02 | 1.91 | 1.72 | 2 | 1.52 | 1.74 | 1.46 | 1.36 |
|  |  |  |  |  |  |  |  |  |  |  |
| pH |  | 7.01 | 7.10 | 7.13 | 6.98 | 7.08 | 8.45 | 7.78 | 8.85 | 7.35 |
| ORP |  |  | -88 | -80 | -273 | -143.3 | -123.4 | -136.3 | -138.9 | -212.4 |
| EC | $\mathrm{uS} / \mathrm{cm}$ | 1034 | 1200 | 1120 | 1263 | 2181 | 1529 | 1269 | 1342 | 1072 |
| T | ${ }^{\circ} \mathrm{C}$ | 11.0 | 12.6 | 8.9 | 15.3 | 9.86 | 14.36 | 9.2 | 13.97 | 8.88 |
| DO | $\mathrm{mg} / \mathrm{l}$ | 0.62 | 0.17 | 0.12 | 0.16 | 0.27 | 0.93 | 1.19 | 0.40 | 3.91 |


|  |  | MW-4 | MW-4 | MW-4 | MW-4 | MW-4 | MW-4 | MW-4 | MW-4 | MW-4 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Units | $07 / 10 / 02$ | $11 / 19 / 02$ | $04 / 23 / 03$ | $11 / 17 / 03$ | $05 / 18 / 04$ | $10 / 9 / 04$ | $5 / 4 / 05$ | $11 / 22 / 05$ | $5 / 9 / 06$ |
| Sulfate | $\mathrm{mg} / \mathrm{l}$ | 165 | 137 | 160 | 128 | 136 | 86.5 | 99.9 | 64.5 | 89.3 |
| Nitrate-Nitrite as N | $\mathrm{mg} / \mathrm{l}$ | 3.97 | 3.27 | 3.59 | 3.93 | 2.7 | 1.47 | 1.53 | 2.22 | 1.28 |
| BOD | $\mathrm{mg} / \mathrm{l}$ | 0.86 | $<6$ | $<2$ | $<2$ | 5.55 | $<2$ | $<2$ | $<2$ | $<2$ |
| Fe (total) | $\mathrm{mg} / \mathrm{l}$ | 33.8 | 27.2 | 35.4 | 12.1 | 1.71 | 18.2 | 2.57 | 18.8 | 0.85 |
| Fe (dissolved) | $\mathrm{mg} / \mathrm{l}$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| Mn (total) | $\mathrm{mg} / /$ | 0.77 | 0.56 | 0.84 | 0.27 | 0.17 | 0.34 | 0.06 | 0.39 | $<0.05$ |
| Mn (dissolved) | $\mathrm{mg} / \mathrm{l}$ | $<0.05$ | $<0.05$ | $<0.05$ | $<0.05$ | $<0.5$ | 0.17 | $<0.05$ | $<0.05$ | $<0.05$ |
|  |  |  |  |  |  |  |  |  |  |  |
| pH |  | 7.24 | 7.36 | 7.29 | 7.18 | 6.96 | 6.5 | 6.99 | 6.78 | 6.86 |
| ORP |  | 268 | 315 | 240 | 46.5 | 44.9 | 52.6 | 741 | 348.6 |  |
| EC | $\mathrm{uS} / \mathrm{cm}$ | 652 | 840 | 870 | 1080 | 957 | 828 | 895 | 11.84 | 646 |
| T | ${ }^{\circ} \mathrm{C}$ | 10.0 | 10.5 | 7.0 | 11.7 | 7.7 | 11.72 | 7.9 | 2.96 | 7.78 |
| DO | $\mathrm{mg} / \mathrm{l}$ | 1.20 | 0.92 | 3.72 | 4.07 | 4.17 | 4.68 | 4.71 | 47.9 | 10.21 |


|  |  | MW-5 | MW-5 | MW-5 | MW-5 | MW-5 | MW-5 | MW-5 | MW-5 | MW-5 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Units | $07 / 10 / 02$ | $11 / 19 / 02$ | $04 / 23 / 03$ | $11 / 17 / 03$ | $05 / 18 / 04$ | $10 / 9 / 04$ | $5 / 4 / 05$ | $11 / 22 / 05$ | $5 / 9 / 06$ |
| Sulfate | $\mathrm{mg} / \mathrm{l}$ | 9.1 | 5.66 | 10.9 | 294 | 88.4 | 10.4 | 141 | 38.4 | 19.7 |
| Nitrate-Nitrite as N | $\mathrm{mg} / \mathrm{l}$ | $<0.1$ | $<0.1$ | $<0.1$ | 5.18 | 0.49 | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| BOD | $\mathrm{mg} / \mathrm{l}$ | 0.82 | 107 | 114 | 89.3 | 21.3 | 66 | 21.7 | 21.8 | 32 |
| Fe (total) | $\mathrm{mg} / \mathrm{l}$ | 30.7 | 23.6 | 37.1 | 38.7 | 15 | 99 | 20.5 | 8 | 7.15 |
| Fe (dissolved) | $\mathrm{mg} / /$ | 6 | 4.8 | 4.26 | 4.7 | 1.09 | 3.14 | $<0.1$ | 4.57 | 6.27 |
| Mn (total) | $\mathrm{mg} / \mathrm{l}$ | 1.96 | 1.56 | 1.83 | 1.41 | 2.87 | 3.73 | 0.92 | 1.06 | 1.11 |
| Mn (dissolved) | $\mathrm{mg} / \mathrm{l}$ | 1.42 | 1.35 | 1.14 | 0.98 | 0.5 | 1.13 | 0.44 | 1.03 | 1.11 |
|  |  |  |  |  |  |  |  |  |  |  |
| pH |  | 6.96 | 7.15 | 7.29 | 6.86 | 7.13 | 7.43 | 7.37 | 8.43 | 6.86 |
| ORP |  | -50 | -90 | -45 | -45.3 | -61.9 | -73.2 | -96.3 | -219.6 |  |
| EC | $\mathrm{uS} / \mathrm{cm}$ | 1137 | 1180 | 1120 | 1988 | 1281 | 1386 | 1295 | 1448 | 1248 |
| T | ${ }^{\circ} \mathrm{C}$ | 9.9 | 11.4 | 6.2 | 12.6 | 7.63 | 12.79 | 7.6 | 13.18 | 7.81 |
| DO | $\mathrm{mg} / \mathrm{l}$ | 0.02 | 0.02 | 0.03 | 2.26 | 3.53 | 3.45 | 3.59 | 0.14 | 3.04 |

Groundwater Quality Monitoring - Selected Biodegradation Parameters (continued)

|  |  | MW-6 | MW-6 | MW-6 | MW-6 | MW-6 | MW-6 | MW-6 | MW-6 | MW-6 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Units | $07 / 10 / 02$ | $11 / 19 / 02$ | $04 / 23 / 03$ | $11 / 17 / 03$ | $05 / 18 / 04$ | $10 / 9 / 04$ | $5 / 4 / 05$ | $11 / 22 / 05$ | $5 / 9 / 06$ |
| Sulfate | $\mathrm{mg} / \mathrm{l}$ | 191 | 201 | 181 | 165 | 126 | 132 | 142 | 138.00 | 133 |
| Nitrate-Nitrite as N | $\mathrm{mg} / \mathrm{l}$ | $<0.1$ | 0.11 | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| BOD | $\mathrm{mg} / \mathrm{l}$ | 0.36 | 18 | 15.2 | 13.6 | 7.4 | 7.35 | 5.07 | 2.8 | 2.54 |
| Fe (total) | $\mathrm{mg} / \mathrm{l}$ | 12.9 | 15.1 | 8 | 70 | 2.79 | 20.7 | 5.21 | 1.99 | 1 |
| Fe (dissolved) | $\mathrm{mg} / \mathrm{l}$ | 0.21 | 0.91 | 0.88 | 1.16 | 0.85 | 0.39 | 0.9 | 0.66 | 0.56 |
| Mn (total) | $\mathrm{mg} / \mathrm{l}$ | 1.77 | 2.2 | 1.94 | 4.11 | 2.05 | 2.09 | 1.2 | 1.49 | 1.46 |
| Mn (dissolved) | $\mathrm{mg} / \mathrm{l}$ | 1.55 | 2.06 | 1.93 | 1.82 | 1.85 | 1.27 | 1.24 | 1.52 | 1.45 |
|  |  |  |  |  |  |  |  |  |  |  |
| pH |  | 7.17 | 7.27 | 7.22 | 7.09 | 7.12 | 7.98 | 7.31 | 7.85 | 7.1 |
| ORP |  | 81 | 46 | -116 | -74 | -102.2 | -96.1 | -8.3 | 23.3 |  |
| EC | $\mathrm{uS} / \mathrm{cm}$ | 1447 | 1780 | 1910 | 2007 | 2239 | 1850 | 1846 | 1776 | 1539 |
| T | ${ }^{\circ} \mathrm{C}$ | 8.5 | 10.2 | 3.6 | 10.8 | 6.6 | 13.36 | 6.9 | 10.65 | 7.14 |
| DO | $\mathrm{mg} / \mathrm{l}$ | 0.09 | 0.62 | 0.20 | 0.37 | 0.83 | 1.69 | 1.99 | 0.25 | 4.42 |


|  |  | MW-7 | MW-7 | MW-7 | MW-7 | MW-7 | MW-7 | MW-7 | MW-7 | MW-7 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Units | $07 / 10 / 02$ | $11 / 19 / 02$ | $04 / 23 / 03$ | $11 / 17 / 03$ | $05 / 18 / 04$ | $10 / 9 / 04$ | $5 / 4 / 05$ | $11 / 22 / 05$ | $5 / 9 / 06$ |
| Sulfate | $\mathrm{mg} / \mathrm{l}$ | 128 | 123 | 121 | 126 | 118 | 108 | 98.8 | 165 | 96.9 |
| Nitrate-Nitrite as N | $\mathrm{mg} / \mathrm{l}$ | 7.12 | 7.11 | 7.33 | 8.48 | 8.61 | 5.65 | 7.44 | 8.05 | 5.4 |
| BOD | $\mathrm{mg} / \mathrm{l}$ | 1.94 | $<6$ | $<2$ | $<2$ | $<2$ | 2.2 | $<2$ | $<2$ | $<2$ |
| Fe (total) | $\mathrm{mg} / \mathrm{l}$ | 31.2 | 38.8 | 119 | 71 | 2.71 | 20.6 | 6.82 | 14.8 | 1.82 |
| Fe (dissolved) | $\mathrm{mg} / \mathrm{l}$ | $<0.1$ | 0.16 | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| Mn (total) | $\mathrm{mg} / \mathrm{l}$ | 1 | 0.81 | 2.98 | 1.81 | 0.19 | 0.35 | 0.13 | 0.29 | 0.05 |
| Mn (dissolved) | $\mathrm{mg} / \mathrm{l}$ | $<0.05$ | $<0.05$ | $<0.05$ | $<0.05$ | $<0.05$ | 0.27 | $<0.05$ | $<0.05$ | $<0.05$ |
|  |  |  |  |  |  |  |  |  |  |  |
| pH | 7.46 | 7.47 | 7.65 | 7.30 | 7.14 | 7.37 | 7.51 | 7.11 | 7.09 |  |
| ORP |  |  | 263 | 276 | 272 | 21.7 | 24.8 | 61.3 | 44.2 | 317.6 |
| EC | uS/cm | 807 | 1200 | 990 | 1032 | 1147 | 1213 | 1131 | 1290 | 921 |
| T | ${ }^{\circ} \mathrm{C}$ | 11.0 | 12.7 | 8.0 | 12.3 | 8.55 | 12.75 | 8.1 | 12.78 | 8.73 |
| DO | $\mathrm{mg} / \mathrm{l}$ | 1.48 | 0.31 | 4.13 | 1.05 | 1.1 | 2.79 | 2.91 | 3.44 | 13.31 |


|  |  | MW-14 | MW-14 | MW-14 | MW-14 | MW-14 | MW-14 | MW-14 | MW-14 | MW-14 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Units | $07 / 10 / 02$ | $11 / 19 / 02$ | $04 / 23 / 03$ | $11 / 17 / 03$ | $05 / 18 / 04$ | $10 / 9 / 04$ | $5 / 4 / 05$ | $11 / 22 / 05$ | $5 / 9 / 06$ |
| Sulfate | $\mathrm{mg} / \mathrm{l}$ | 18.4 | 10.2 | 27.6 | 13.8 | 37.2 | 16.4 | 65.9 | 75.3 | 50.5 |
| Nitrate-Nitrite as N | $\mathrm{mg} / \mathrm{l}$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| BOD | $\mathrm{mg} / \mathrm{l}$ | 5.61 | 164 | 130 | 190 |  | 78 | 41.1 | 32.8 | 46.7 |
| Fe (total) | $\mathrm{mg} / \mathrm{l}$ | 124 | 38 | 52 | 47 | 62 | 35.9 | 8.09 | 10.1 | 13.2 |
| Fe (dissolved) | $\mathrm{mg} / \mathrm{l}$ | $<0.1$ | 1.01 | 1.43 | 3.18 | 7 | 1.48 | 0.18 | 5.33 | 12.2 |
| Mn (total) | $\mathrm{mg} / \mathrm{l}$ | 9.6 | 3.61 | 3.98 | 3.66 | 15.6 | 1.86 | 0.56 | 0.68 | 0.94 |
| Mn (dissolved) | $\mathrm{mg} / \mathrm{I}$ | 0.36 | 1.81 | 1.51 | 1.13 | 0.92 | 0.66 | 0.48 | 0.56 | 0.94 |
|  |  |  |  |  |  |  |  |  |  |  |
| pH |  | 7.07 | 7.19 | 7.23 | 7.02 | 7.21 | 7.79 | 7.69 | 8.78 | 6.87 |
| ORP |  | -40 | -40 | -186 | -135 | -91.1 | -96.7 | -132.2 | -223.9 |  |
| EC | $\mathrm{uS} / \mathrm{cm}$ | 1502 | 1880 | 1740 | 1758 | 1930 | 2421 | 2416 | 2267 | 18.53 |
| T | ${ }^{\circ} \mathrm{C}$ | 11.5 | 13.7 | 8.1 | 17.7 | 11.91 | 17.74 | 9.41 | 15.87 | 9.76 |
| DO | $\mathrm{mg} / \mathrm{I}$ | 1.10 | 0.13 | 0.04 | 0.22 | 0.39 | 0.64 | 0.73 | 0.26 | 1.78 |

Groundwater Quality Monitoring - Selected Biodegradation Parameters (continued)

|  |  | MW-16 | MW-16 | MW-16 | MW-16 | MW-16 | MW-16 | MW-16 | MW-16 | MW-16 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Units | $07 / 10 / 02$ | $11 / 19 / 02$ | $04 / 23 / 03$ | $11 / 17 / 03$ | $05 / 18 / 04$ | $10 / 9 / 04$ | $5 / 4 / 05$ | $11 / 2 / 05$ | $5 / 9 / 06$ |
| Sulfate | $\mathrm{mg} / \mathrm{l}$ | 110 | 167 | 53.6 | 33.9 | 60.9 | 25.5 | 36.7 | 79.2 | 126 |
| Nitrate-Nitrite as N | $\mathrm{mg} / \mathrm{I}$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| BOD | $\mathrm{mg} / \mathrm{l}$ | 2.27 | 69 | 62.4 | 93.5 | 42 | 54 | 37.7 | 36 | 39 |
| Fe (total) | $\mathrm{mg} / \mathrm{I}$ | 20.1 | 15.7 | 40.8 | 22.6 | 2.29 | 107 | 78.7 | 15.2 | 1.34 |
| Fe (dissolved) | $\mathrm{mg} / \mathrm{I}$ | $<0.1$ | $<0.1$ | 0.18 | 0.18 | 0.4 | $<0.1$ | 0.52 | 0.44 | 0.38 |
| Mn (total) | $\mathrm{mg} / /$ | 1.96 | 2.03 | 2.1 | 1.86 | 1.65 | 3.91 | 3.85 | 2.36 | 2.02 |
| Mn (dissolved) | $\mathrm{mg} / \mathrm{I}$ | 0.59 | 1.66 | 1.38 | 1.67 | 1.63 | 1.81 | 1.97 | 2.05 | 1.9 |
|  |  |  |  |  |  |  |  |  |  |  |
| pH | 7.09 | 7.24 | 7.19 | 6.95 | 7.01 | 7.94 | 7.31 | 7.97 | 6.76 |  |
| ORP |  |  | 230 | 228 | -62 | -107.5 | -69.9 | -63.1 | -18.1 | -42.9 |
| EC | uS/cm | 1404 | 1760 | 1510 | 1795 | 2241 | 2030 | 2137 | 2134 | 1926 |
| T | ${ }^{\circ} \mathrm{C}$ | 10.8 | 11.6 | 5.2 | 11.7 | 7.27 | 12.93 | 7.36 | 11.15 | 7.32 |
| DO | $\mathrm{mg} / \mathrm{l}$ | 0.18 | 0.33 | 0.02 | 0.38 | 0.55 | 1.06 | 1.29 | 0.21 | 3.35 |


|  |  | MW-17 | MW-17 | MW-17 | MW-17 | MW-17 | MW-17 | MW-17 | MW-17 | MW-17 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Units | $07 / 10 / 02$ | $11 / 19 / 02$ | $04 / 23 / 03$ | $11 / 17 / 03$ | $05 / 18 / 04$ | $10 / 9 / 04$ | $5 / 4 / 05$ | $11 / 22 / 05$ | $5 / 9 / 06$ |
| Sulfate | $\mathrm{mg} / \mathrm{I}$ | 55.4 | 76.8 | 43 | 38 | 39.1 | 37.6 | 49.6 | 87.3 | 56 |
| Nitrate-Nitrite as N | $\mathrm{mg} / \mathrm{l}$ | $<0.1$ | $<0.1$ | $<0.1$ | 0.1 | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| BOD | $\mathrm{mg} / \mathrm{l}$ | 0.32 | $<6$ | $<2$ | $<2$ | 10.2 | $<2$ | $<2$ | 4.26 | $<2$ |
| Fe (total) | $\mathrm{mg} / \mathrm{I}$ | 6.9 | 11 | 7.3 | 142 | 1.38 | 79 | 19.1 | 30.8 | 2.75 |
| Fe (dissolved) | $\mathrm{mg} / \mathrm{I}$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ | $<0.1$ |
| Mn (total) | $\mathrm{mg} / \mathrm{I}$ | 0.71 | 1.03 | 0.97 | 4.7 | 1.38 | 3.43 | 1.42 | 2.71 | 0.82 |
| Mn (dissolved) | $\mathrm{mg} / \mathrm{l}$ | 0.48 | 0.78 | 0.44 | 0.71 | 0.69 | 0.6 | $<0.05$ | 0.66 | 0.58 |
|  |  |  |  |  |  |  |  |  |  |  |
| pH |  | 7.27 | 7.38 | 7.31 | 7.14 | 7.14 | 7.41 | 7.39 | 7.54 | 6.86 |
| ORP |  | 279 | 264 | 19 | 7.9 | 23.2 | 27.9 | 43.2 | 118.1 |  |
| EC | $\mathrm{uS} / \mathrm{cm}$ | 838 | 1150 | 1070 | 1203 | 1292 | 1417 | 1491 | 1351 | 1111 |
| T | ${ }^{\circ} \mathrm{C}$ | 10.0 | 10.2 | 5.4 | 10.9 | 6.33 | 12.65 | 7.49 | 11.03 | 6.74 |
| DO | $\mathrm{mg} / \mathrm{l}$ | 1.20 | 1.27 | 0.12 | 0.29 | 0.43 | 1.51 | 1.69 | 0.62 | 5.65 |


| Well ID | Date | pH | EC | T | DO | ORP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | uS/cm | ${ }^{\circ} \mathrm{C}$ | mg/l | mV |
| MW-1 | 04/08/02 | 7.19 | 1278 | 6.2 | 0.05 | -11.7 |
| MW-1 | 11/19/02 | 7.10 | 1045 | 13.9 | 0.17 | -88.0 |
| MW-1 | 04/23/03 | 7.13 | 1218 | 8.9 | 0.12 | -80.0 |
| MW-1 | 11/17/03 | 6.98 | 1263 | 15.3 | 0.16 | -272.6 |
| MW-1 | 05/18/04 | 7.08 | 2181 | 9.9 | 0.27 | -143.3 |
| MW-1 | 10/09/04 | 8.45 | 1529 | 14.4 | 0.93 | -123.4 |
| MW-1 | 05/02/05 | 7.78 | 1269 | 9.2 | 1.19 | -136.3 |
| MW-1 | 11/22/05 | 8.85 | 1342 | 14.0 | 0.40 | -138.9 |
| MW-1 | 05/09/06 | 7.35 | 1072 | 8.9 | 3.91 | -212.4 |
| MW-2 | 04/09/02 | 7.18 | 1283 | 11.1 | 0.00 | -16.4 |
| MW-2 | 11/19/02 | 7.37 | 866 | 16.1 | 0.07 | -150.0 |
| MW-2 | 04/23/03 | 7.36 | 1078 | 12.4 | 0.03 | -81.0 |
| MW-2 | 11/17/03 | 7.15 | 9.15 | 12.9 | 0.12 | -172.8 |
| MW-2 | 05/18/04 | 7.32 | 1816 | 11.5 | 0.42 | -33.0 |
| MW-2 | 10/09/04 | 8.48 | 1753 | 17.4 | 0.56 | -132.3 |
| MW-2 | 05/02/05 | 7.93 | 1810 | 10.1 | 0.79 | -129.1 |
| MW-2 | 11/22/05 | 8.16 | 1077 | 14.2 | 0.34 | -34.1 |
| MW-2 | 05/09/06 | 7.13 | 1299 | 10.4 | 1.54 | 64.1 |
| MW-3 | 04/09/02 | 7.28 | 950 | 11.6 | 0.07 | -20.0 |
| MW-3 | 11/19/02 | 7.18 | 826 | 14.2 | 0.33 | 110.0 |
| MW-3 | 04/23/03 | 7.44 | 1021 | 9.4 | 0.64 | 141.0 |
| MW-3 | 11/17/03 | 7.22 | 915 | 12.4 | 0.41 | -76.0 |
| MW-3 | 05/18/04 | 7.21 | 1013 | 9.0 | 0.52 | 6.3 |
| MW-3 | 10/09/04 | 7.49 | 1010 | 12.3 | 0.65 | 4.1 |
| MW-3 | 05/02/05 | 7.31 | 965 | 9.4 | 0.87 | 12.7 |
| MW-3 | 11/22/05 | 7.71 | 1011 | 13.3 | 0.13 | 9.7 |
| MW-3 | 05/09/06 | 6.8 | 822 | 9.1 | 2.36 | 51.7 |
| MW-4 | 04/08/02 | 7.66 | 763 | 7.4 | 0.79 | -38.5 |
| MW-4 | 11/19/02 | 7.36 | 674 | 11.5 | 0.92 | 268.0 |
| MW-4 | 04/23/03 | 7.29 | 874 | 7.0 | 3.72 | 315.0 |
| MW-4 | 11/17/03 | 7.18 | 1080 | 11.7 | 4.07 | 239.5 |
| MW-4 | 05/18/04 | 6.96 | 957 | 7.7 | 4.17 | 46.5 |
| MW-4 | 10/09/04 | 6.5 | 828 | 11.7 | 4.68 | 44.9 |
| MW-4 | 05/02/05 | 6.99 | 895 | 7.9 | 4.71 | 52.6 |
| MW-4 | 11/22/05 | 6.78 | 741 | 11.8 | 2.96 | 47.9 |
| MW-4 | 05/09/06 | 6.86 | 646 | 7.8 | 10.21 | 348.6 |
| MW-5 | 04/08/02 | 7.28 | 1376 | 7.6 | 0.06 | -16.8 |
| MW-5 | 11/19/02 | 7.11 | 1123 | 12.0 | 0.02 | -50.0 |
| MW-5 | 04/23/03 | 7.29 | 1353 | 6.2 | 0.03 | -90.0 |
| MW-5 | 11/17/03 | 6.86 | 1988 | 12.6 | 2.26 | -45.2 |
| MW-5 | 05/18/04 | 7.13 | 1281 | 7.6 | 3.53 | -45.3 |
| MW-5 | 10/09/04 | 7.43 | 1386 | 12.8 | 3.45 | -61.9 |
| MW-5 | 05/02/05 | 7.37 | 1295 | 7.6 | 3.59 | -73.2 |
| MW-5 | 11/22/05 | 8.43 | 1448 | 13.2 | 0.14 | -96.3 |
| MW-5 | 05/09/06 | 6.86 | 1248 | 7.8 | 3.04 | -219.6 |
| MW-6 | 04/08/02 | 6.23 | 1889 | 6.7 | 0.03 | -24.2 |
| MW-6 | 11/19/02 | 7.27 | 1497 | 8.8 | 0.62 | 80.9 |
| MW-6 | 04/23/03 | 7.22 | 2181 | 3.6 | 0.20 | 46.0 |
| MW-6 | 11/17/03 | 7.09 | 2007 | 10.8 | 0.37 | -115.8 |
| MW-6 | 05/18/04 | 7.12 | 2239 | 6.6 | 0.83 | -74.0 |
| MW-6 | 10/09/04 | 7.98 | 1850 | 13.4 | 1.69 | -102.2 |
| MW-6 | 05/02/05 | 7.31 | 1846 | 6.9 | 1.99 | -96.1 |
| MW-6 | 11/22/05 | 7.85 | 1776 | 10.7 | 0.25 | -8.3 |
| MW-6 | 05/09/06 | 7.1 | 1539 | 7.1 | 4.42 | 23.3 |

Groundwater Quality Monitoring - Field-Measured Parameters

| Well ID | Date | pH | $\begin{gathered} \mathrm{EC} \\ \mathrm{uS} / \mathrm{cm} \end{gathered}$ | $\begin{aligned} & \mathrm{T} \\ & { }^{\mathrm{T}} \mathrm{C} \end{aligned}$ | $\begin{gathered} \mathrm{DO} \\ \mathrm{mg} / \mathrm{l} \end{gathered}$ | $\begin{gathered} \mathrm{ORP} \\ \mathrm{mV} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MW-7 | 04/08/02 | 7.73 | 980 | 8.2 | 1.19 | -43.5 |
| MW-7 | 11/19/02 | 7.47 | 835 | 12.1 | 0.31 | 263.0 |
| MW-7 | 04/23/03 | 7.65 | 1106 | 8.0 | 4.13 | 276.0 |
| MW-7 | 11/17/03 | 7.30 | 1032 | 12.3 | 1.05 | 271.6 |
| MW-7 | 05/18/04 | 7.14 | 1147 | 8.6 | 1.10 | 21.7 |
| MW-7 | 10/09/04 | 7.37 | 1213 | 12.8 | 2.79 | 24.8 |
| MW-7 | 05/02/05 | 7.51 | 1131 | 8.1 | 2.91 | 61.3 |
| MW-7 | 11/22/05 | 7.11 | 1290 | 12.8 | 3.44 | 44.2 |
| MW-7 | 05/09/06 | 7.09 | 921 | 8.7 | 13.31 | 317.6 |
| MW-8 | 04/08/02 | 7.58 | 1873 | 7.3 | 1.38 | -34.0 |
| MW-8 | 11/19/02 | 7.39 | 1552 | 12.2 | 0.17 | 301.0 |
| MW-8 | 04/23/03 | 7.66 | 1967 | 7.3 | 1.94 | 255.0 |
| MW-8 | 11/17/03 | 7.40 | 1775 | 12.5 | 0.60 | 247.4 |
| MW-8 | 05/18/04 | 7.44 | 1805 | 7.6 | 2.03 | 21.3 |
| MW-8 | 10/09/04 | 7.44 | 1950 | 12.2 | 2.16 | 24.2 |
| MW-8 | 05/02/05 | 7.58 | 1801 | 7.9 | 2.29 | 160.1 |
| MW-8 | 11/22/05 | 7.45 | 1830 | 12.3 | 0.33 | 40.7 |
| MW-8 | 05/09/06 | 7.28 | 1542 | 7.8 | 10.33 | 271.7 |
| MW-9 | 04/08/02 | 7.64 | 1296 | 7.0 | 1.89 | -37.7 |
| MW-9 | 11/19/02 | 7.57 | 1059 | 11.6 | 1.56 | 290.0 |
| MW-9 | 04/23/03 | 7.62 | 1362 | 6.5 | 3.09 | 275.0 |
| MW-9 | 11/17/03 | 7.36 | 1263 | 11.4 | 1.73 | 155.0 |
| MW-9 | 05/18/04 | 7.39 | 781 | 7.2 | 0.46 | -13.2 |
| MW-9 | 10/09/04 | 7.57 | 1134 | 11.9 | 1.37 | 18.5 |
| MW-9 | 05/02/05 | 7.61 | 1197 | 7.2 | 2.41 | 36.9 |
| MW-9 | 11/22/05 | 7.56 | 1385 | 11.5 | 0.42 | 41.8 |
| MW-9 | 05/09/06 | 7.01 | 1180 | 7.3 | 8.46 | 254.0 |
| MW-10 | 04/08/02 | 7.36 | 1583 | 7.7 | 0.02 | -21.2 |
| MW-10 | 11/19/02 | 7.25 | 1500 | 12.9 | 0.02 | -109.0 |
| MW-10 | 04/23/03 | 7.47 | 1684 | 8.7 | 0.05 | 125.0 |
| MW-10 | 11/17/03 | 7.03 | 1456 | 13.1 | 0.18 | -161.3 |
| MW-10 | 05/18/04 | 7.27 | 1539 | 7.7 | 0.58 | -94.6 |
| MW-10 | 10/09/04 | 7.77 | 1668 | 12.7 | 1.36 | -26.2 |
| MW-10 | 05/02/05 | 7.13 | 1563 | 7.9 | 1.42 | -19.1 |
| MW-10 | 11/22/05 | 8.67 | 1616 | 12.4 | 0.38 | -63.2 |
| MW-10 | 05/09/06 | 7.07 | 1402 | 8.3 | 2 | -239.8 |
| MW-11 | 07/23/02 | 7.01 | 800 | 15.4 | 0.00 |  |
| MW-11 | 11/19/02 | 7.06 | 962 | 14.7 | 0.23 | 266.0 |
| MW-11 | 04/23/03 | 7.07 | 1211 | 7.4 | 0.45 | 284.0 |
| MW-11 | 11/17/03 | 7.13 | 951 | 14.7 | 0.27 | -104.0 |
| MW-11 | 05/18/04 | 7.01 | 1935 | 8.5 | 1.24 | 21.5 |
| MW-11 | 10/09/04 | 7.7 | 1496 | 15.1 | 1.38 | -41.9 |
| MW-11 | 05/02/05 | 7.09 | 1595 | 8.8 | 1.49 | -51.2 |
| MW-11 | 11/22/05 | 7.67 | 2136 | 14.1 | 3.65 | 22.4 |
| MW-11 | 05/09/06 | 6.85 | 1637 | 8.3 | 5.28 | 39.7 |
| MW-12 | 07/23/02 | 7.06 | 1100 | 15.4 | 0.00 |  |
| MW-12 | 11/19/02 | 7.18 | 1000 | 13.6 | 0.02 | -80.0 |
| MW-12 | 04/23/03 | 7.26 | 1543 | 7.8 | 0.00 | 8.3 |
| MW-12 | 11/17/03 | 7.00 | 1442 | 14.5 | 0.18 | -185.0 |
| MW-12 | 05/18/04 | 7.88 | 1339 | 8.9 | 0.81 | -109.9 |
| MW-12 | 10/09/04 | 8.02 | 1907 | 14.3 | 0.64 | -85.2 |
| MW-12 | 05/02/05 | 7.91 | 1714 | 9.2 | 0.97 | -91.3 |
| MW-12 | 11/22/05 | 8.33 | 2133 | 13.7 | 0.52 | -82.4 |
| MW-12 | 05/09/06 | 6.87 | 1772 | 8.8 | 2.25 | -206.7 |


| Well ID | Date | pH | $\begin{gathered} \mathrm{EC} \\ \mathrm{uS} / \mathrm{cm} \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ { }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} \mathrm{DO} \\ \mathrm{mg} / \mathrm{l} \end{gathered}$ | $\begin{gathered} \hline \text { ORP } \\ \mathrm{mV} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MW-13 | 07/10/02 | 7.00 | 1881 | 10.5 | 0.30 |  |
| MW-13 | 11/19/02 | 7.27 | 1930 | 14.4 | 0.11 | -17.0 |
| MW-13 | 04/23/03 | 7.17 | 2212 | 8.0 | 0.29 | 10.7 |
| MW-13 | 11/17/03 | 7.16 | 1098 | 14.5 | 0.17 | -149.8 |
| MW-13 | 05/18/04 | 7.18 | 1229 | 11.3 | 0.94 | -81.6 |
| MW-13 | 10/09/04 | 8.22 | 1684 | 18.1 | 0.77 | -88.8 |
| MW-13 | 05/02/05 | 7.29 | 1615 | 10.0 | 0.99 | -100.1 |
| MW-13 | 11/22/05 | 8.29 | 1101 | 14.8 | 0.2 | -33.4 |
| MW-13 | 05/09/06 | 7.07 | 1039 | 9.2 | 2.01 | -102.7 |
| MW-14 | 07/23/02 | 7.30 | 1900 | 15.9 | 1.10 |  |
| MW-14 | 11/19/02 | 7.19 | 1703 | 14.3 | 0.13 | -40.0 |
| MW-14 | 04/23/03 | 7.23 | 1989 | 8.1 | 0.04 | -40.0 |
| MW-14 | 11/17/03 | 7.02 | 1758 | 17.7 | 0.22 | -186.0 |
| MW-14 | 05/18/04 | 7.21 | 1930 | 11.9 | 0.39 | -135.0 |
| MW-14 | 10/09/04 | 7.79 | 2421 | 17.7 | 0.64 | -91.1 |
| MW-14 | 05/02/05 | 7.69 | 2416 | 9.4 | 0.73 | -96.7 |
| MW-14 | 11/22/05 | 8.78 | 2267 | 15.9 | 0.26 | -132.2 |
| MW-14 | 05/09/06 | 6.87 | 2160 | 9.8 | 1.78 | -223.9 |
| MW-15 | 07/23/02 | 7.03 | 1100 | 15.5 | 0.09 |  |
| MW-15 | 11/19/02 | 7.27 | 930 | 15.1 | 0.05 | -70.0 |
| MW-15 | 04/23/03 | 7.28 | 1153 | 9.4 | 0.01 | -73.0 |
| MW-15 | 11/17/03 | 6.96 | 1394 | 18.3 | 0.18 | -183.0 |
| MW-15 | 05/18/04 | 7.34 | 1793 | 11.6 | 0.42 | -147.2 |
| MW-15 | 10/09/04 | 7.9 | 1986 | 17.8 | 0.87 | -85.7 |
| MW-15 | 05/02/05 | 7.67 | 1994 | 10.0 | 0.91 | -81.3 |
| MW-15 | 11/22/05 | 8.38 | 2350 | 15.3 | 0.3 | -48.4 |
| MW-15 | 05/09/06 | 7.24 | 2093 | 9.8 | 2.39 | -24.5 |
| MW-16 | 07/10/02 | 7.09 | 1404 | 10.8 | 0.18 |  |
| MW-16 | 11/19/02 | 7.24 | 1388 | 10.5 | 0.33 | 230.0 |
| MW-16 | 04/23/03 | 7.19 | 1829 | 5.2 | 0.02 | 228.0 |
| MW-16 | 11/17/03 | 6.95 | 1795 | 11.7 | 0.38 | -62.3 |
| MW-16 | 05/18/04 | 7.01 | 2241 | 7.3 | 0.55 | -107.5 |
| MW-16 | 10/09/04 | 7.94 | 2030 | 12.9 | 1.06 | -69.9 |
| MW-16 | 05/02/05 | 7.31 | 2137 | 7.4 | 1.29 | -63.1 |
| MW-16 | 11/22/05 | 7.97 | 2134 | 11.2 | 0.21 | -18.1 |
| MW-16 | 05/09/06 | 6.76 | 1926 | 7.3 | 3.35 | -42.9 |
| MW-17 | 07/10/02 | 7.27 | 838 | 10.0 | 1.20 |  |
| MW-17 | 11/19/02 | 7.38 | 882 | 10.5 | 1.27 | 279.0 |
| MW-17 | 04/23/03 | 7.31 | 1218 | 5.4 | 0.12 | 264.0 |
| MW-17 | 11/17/03 | 7.14 | 1203 | 10.9 | 0.29 | 19.2 |
| MW-17 | 05/18/04 | 7.14 | 1292 | 6.3 | 0.43 | 7.9 |
| MW-17 | 10/09/04 | 7.41 | 1417 | 12.7 | 1.51 | 23.2 |
| MW-17 | 05/02/05 | 7.39 | 1491 | 7.5 | 1.69 | 27.9 |
| MW-17 | 11/22/05 | 7.54 | 1351 | 11.0 | 0.62 | 43.2 |
| MW-17 | 05/09/06 | 6.86 | 1111 | 6.7 | 5.65 | 118.1 |

## APPENDIX G

## SUMMARY OF ANALYTICAL DATA - SYSTEM MONITORING

APPENDIX G-1

## WATER QUALITY

| Extraction wellfield HR 2, 3, 4, and 5 |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | VLS | VLS | VLS | VLS | VLS | VLS | VLS | VLS | VLS | VLS | VLS |
| VLS | $07 / 11 / 02$ | $07 / 16 / 02$ | $07 / 23 / 02$ | $08 / 15 / 02$ | $09 / 18 / 02$ | $09 / 24 / 02$ | $10 / 02 / 02$ | $10 / 16 / 02$ | $11 / 18 / 02$ | $12 / 16 / 02$ | $01 / 07 / 03$ |  |
| MBTE | ppb | $<100$ | $<200$ | $<200$ | $<200$ | $<50$ | $<100$ | $<200$ | $<100$ | $<25$ | $<20$ | $<20$ |
| Benzene | ppb | 14100 | 8030 | 6570 | 7730 | 4260 | 4620 | 3750 | 2530 | 1150 | 1235 | 1016 |
| Toluene | ppb | 12200 | 9390 | 8940 | 12100 | 6060 | 8630 | 6380 | 4060 | 1820 | 1917 | 1641 |
| Ethylbenzene | ppb | 1130 | 879 | 825 | 1340 | 621 | 1310 | 764 | 433 | 242 | 180.3 | 155 |
| Xylenes (Total) | ppb | 5300 | 3950 | 3940 | 7280 | 4110 | 8080 | 5740 | 4080 | 2820 | 236 | 2109 |
| Phenols (Total) | ppb | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
| GRO (TPH) | $\mathrm{mg} / \mathrm{l}$ | 74.3 | 57.0 | 51.5 | 68.8 | 35.2 | 67.7 | 44.1 | 30.7 | 20.7 | 15.1 | 12.6 |


| OWS |  | OWS | OWS | OWS | OWS | OWS | OWS | OWS | OWS | OWS | OWS |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $07 / 11 / 02$ | $07 / 16 / 02$ | $07 / 23 / 02$ | $08 / 15 / 02$ | $09 / 18 / 02$ | $09 / 24 / 02$ | $10 / 02 / 02$ | $11 / 18 / 02$ | $12 / 16 / 02$ | $01 / 07 / 03$ |  |
| MBTE | ppb | $<200$ | $<200$ | $<200$ | $<200$ | $<50$ | $<50$ | $<50$ | $<20$ | $<50$ |  |
| Benzene | ppb | 14700 | 8150 | 6660 | 7910 | 4370 | 3940 | 947 | 1160 | 1080 |  |
| Toluene | ppb | 12600 | 9370 | 8850 | 12500 | 5860 | 8840 | 2180 | 1600 | 1540 |  |
| Ethylbenzene | ppb | 1160 | 826 | 814 | 1720 | 604 | 1310 | 342 | 148 | 99.9 |  |
| Xylenes (Total) | ppb | 5450 | 3770 | 3920 | 7820 | 4130 | 7850 | 2640 | 2100 | 1830 |  |
| Phenols (Total) | ppb | 365 | NA | NA | NA | NA | NA | NA | NA | NA |  |
| GRO (TPH) | $\mathrm{mg} / 1$ | 73.9 | 59.1 | 50.7 | 68.2 | 35.6 | 52.3 | 19.6 | 15.7 | 15.1 |  |


| AS |  | AS | AS | AS | AS | AS | AS |  | AS | AS | AS | AS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Flow to stripper | gpm | 15.4 | 16.3 | 14.8 | 15.5 | 29.1 | 29.2 |  | 10.6 | 11.9 | 12.3 | 12.2 |
|  |  | 07/11/02 | 07/16/02 | 07/23/02 | 08/15/02 | 09/18/02 | 09/24/02 |  | 10/16/02 | 11/18/02 | 12/16/02 | 01/07/03 |
| MBTE | ppb | <5 | $<1$ | $<1$ | 1.6 | $<1$ | <10 |  | $<1$ | $<1$ | $<1$ |  |
| Benzene | ppb | 63.6 | 13.2 | 5 | 5.9 | 49.7 | 209 |  | 4.6 | 7.5 | 3.1 |  |
| Toluene | ppb | 75.1 | 16 | 7.3 | 9 | 70.3 | 466 |  | 7.6 | 5.6 | 2.7 |  |
| Ethylbenzene | ppb | 14.1 | 2.2 | 2.1 | 2.7 | 6.7 | 97.8 |  | 3.3 | 4.7 | 4.3 |  |
| Xylenes (Total) | ppb | 62.9 | 11.9 | 8.1 | 13.8 | 68.4 | 659 |  | 13.8 | 15.7 | 11.2 |  |
| Phenols (Total) | ppb | NA | NA | NA | NA | NA | NA |  | NA | NA | NA |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Effluent |  | $\begin{aligned} & \hline \text { Effluent } \\ & 07 / 11 / 02 \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 07 / 16 / 02 \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 07 / 23 / 02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Effluent } \\ & 08 / 15 / 02 \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & \text { 09/18/02 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & \text { 09/24/02 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & \text { 10/02/02 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 10 / 16 / 02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 11 / 18 / 02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 12 / 16 / 02 \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 01 / 07 / 03 \end{aligned}$ |
| MBTE | ppb | <5 | <1 | <1 | 2.4 | $<1$ | <10 | $<1$ | <1 | <1 | $<1$ | $<1$ |
| Benzene | ppb | 66.1 | 10.4 | 3.2 | 11.6 | 36.8 | 198.0 | 7.1 | 3.7 | 4.1 | 2.3 | 2.2 |
| Toluene | ppb | 65.8 | 12.2 | 4.6 | 18.1 | 50.5 | 445.0 | 17.5 | 6.2 | 3.3 | 1.8 | 3.7 |
| Ethylbenzene | ppb | 9.2 | 1.9 | $<1$ | 4.4 | 5.8 | 99.9 | 6.2 | 3.3 | 3.3 | 2.4 | 2.2 |
| Xylenes (Total) | ppb | 52.7 | 9.2 | 4.8 | 26.3 | 52.6 | 653.0 | 49.8 | 11.8 | 6.5 | 7.2 | 10.7 |
| Phenols (Total) | ppb | 335 | 355 | NA | 316 | 296 | 238 | NA | 207 | 207 | 160 | 152 |
| GRO (TPH) | $\mathrm{mg} / \mathrm{l}$ | 1.91 | 0.60 | 0.43 | 1.08 | 0.81 | 5.98 | 0.61 | 0.61 | 1.20 | 0.52 | 0.48 |
|  |  | Effluent <br> 07/11/02 | $\begin{aligned} & \hline \text { Effluent } \\ & 07 / 16 / 02 \end{aligned}$ | Effluent <br> 08/15/02 | Effluent09/18/02 |  | $\begin{aligned} & \hline \text { Effluent } \\ & \text { 09/24/02 } \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 10 / 02 / 02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Effluent } \\ & 10 / 16 / 02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 11 / 18 / 02 \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 12 / 16 / 02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 01 / 07 / 03 \\ & \hline \end{aligned}$ |
| Selected Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\overline{\mathrm{Fe}}$ (total) | mg/l | 13.7 | 9.0 | $<0.1$ |  | 3.3 | 1.4 |  | 1.3 | 1.5 | 6.1 | 6.2 |
| Mn (total) | $\mathrm{mg} / \mathrm{l}$ | 1.61 | 1.44 | 0.98 |  | 1.1 | 0.9 |  | 1.1 | 1.1 | 1.0 | 1.0 |
| TSS | $\mathrm{mg} / \mathrm{l}$ | 426 | 340 | 506 |  | 103 | 27 |  | 35 | 17 | 267 | 203 |
| pH |  | 8.16 | 8.18 | 3.83 |  | 8.38 | 8.34 | 8.44 | 8.54 | 8.29 | 8.44 | 8.45 |
| EC | uS/cm | 1100 | 1000 | 1200 |  | 1100 | 1140 | 1130 | 1240 | 1140 | 1170 | 1170 |
| T | ${ }^{\circ} \mathrm{C}$ | 15.5 | 18.6 | 19.1 |  | 17.5 | 17.6 | 14.3 | 14.9 | 16.3 | 12.6 | 14.8 |

Extraction wellfield HR-2, 3, 4, and 5

| Extraction wellfield HR 4,5,6, and 7 |
| :---: |
| VLS VLS VLS |


| VLS | VLS | VLS | VLS | VLS | VLS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $07 / 22 / 03$ | $08 / 21 / 03$ | $09 / 23 / 03$ | $10 / 22 / 03$ | $11 / 17 / 03$ | $12 / 17 / 03$ |
| $<10$ | $<100$ | $<20$ | $<5$ | $<50$ | $<20$ |
| 655 | 843.8 | 877.7 | 265 | 290 | 137 |
| 3290 | 3538 | 3476 | 1093 | 555.4 | 285.8 |
| 248 | 522.1 | 392 | 149.2 | 111.5 | 56.4 |
| 3310 | 3897 | 3084 | 2468 | 1940 | 1485 |
| NA | NA | NA | NA | NA | NA |
| 15.0 | $<20$ | 15.1 | 9.7 | 10.0 | 4.9 |
|  |  |  |  |  |  |
| Effluent | Effluent | Effluent | Effluent | Effluent | Effluent |
| $07 / 22 / 03$ | $08 / 21 / 03$ | $09 / 23 / 03$ | $10 / 22 / 03$ | $11 / 17 / 03$ | $12 / 17 / 03$ |
| $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ |
| $<1$ | 1 | 2.3 | $<1$ | $<1$ | 1.0 |
| 3 | 3.8 | 4.9 | $<1$ | 1.4 | 1.4 |
| $<1$ | 1.6 | 2.2 | $<1$ | $<1$ | 3.4 |
| 6.6 | 8.9 | 12.5 | 3.7 | 5.8 | 10.7 |
| 52.2 | 149 | 114 | 70.3 | 58.8 | 43.9 |
| $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.3$ |


| Effluent | Effluent | Effluent | Effluent | Effluent | Effluent |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 07/22/03 | $08 / 21 / 03$ | $09 / 23 / 03$ | $10 / 22 / 03$ | $11 / 17 / 03$ | $12 / 17 / 03$ |
| 6.10 | 0.98 | 1.5 | 2.6 | 2.33 | 0.85 |
| 0.96 | 0.78 | 1.03 | 0.79 | 0.76 | 0.75 |
| 354 | 185 | 29 | 14 | 87 | 32 |
| 8.1 | 8 | 7.86 | NM | NM | NM |
| 1125 | 1144 | 1101 | NM | NM | NM |
| 20.0 | 16.5 | 17.1 | NM | NM | NM |


| VLS |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | VLS | VLS | VLS | VLS | VLS |  |
|  | 03/28/03 | $04 / 23 / 03$ | $05 / 19 / 03$ | $06 / 17 / 03$ | $07 / 15 / 03$ |  |
| MBTE | ppb | $<200$ | $<50$ | $<50$ | $<20$ | $<10$ |
| Benzene | ppb | 4120 | 1390 | 1350 | 503 | 458 |
| Toluene | ppb | 5260 | 2670 | 2320 | 747 | 632 |
| Ethylbenzene | ppb | 857 | 278 | 202 | 61.7 | 41.3 |
| Xylenes (Total) | ppb | 6240 | 3000 | 2180 | 836 | 720 |
| Phenols (Total) | ppb | NA | NA | NA | NA | NA |
| GRO (TPH) | $\mathrm{mg} / \mathrm{I}$ | 53.4 | 16.2 | 14.8 | 4.9 | 3.4 |


| Effluent |  | Effluent <br> $03 / 28 / 03$ | Effluent <br> $04 / 23 / 03$ | Effluent <br> $05 / 19 / 03$ | Effluent <br> $06 / 17 / 03$ | Effluent <br> $07 / 15 / 03$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| MBTE | ppb | $<20$ | $<1$ | $<1$ | $<1$ | $<1$ |
| Benzene | ppb | 23 | 3.2 | 2.2 | $<1$ | $<1$ |
| Toluene | ppb | 34.8 | 5 | 3.4 | $<1$ | $<1$ |
| Ethylbenzene | ppb | 61.1 | 3.2 | $<1$ | $<1$ | $<1$ |
| Xylenes (Total) | ppb | 183.0 | 15.2 | 4.7 | $<3$ | $<3$ |
| Phenols (Total) | ppb | 181 | 394 | 236 | 140 | 130 |
| GRO (TPH) | $\mathrm{mg} / \mathrm{I}$ | 15.00 | 0.90 | 0.23 | $<0.2$ | $<0.2$ |


| Selected Parameters | Effluent <br> 03/28/03 | Effluent <br> $04 / 23 / 03$ | Effluent <br> $05 / 19 / 03$ | Effluent <br> $06 / 17 / 03$ | Effluent <br> $07 / 15 / 03$ |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Fe (total) | $\mathrm{mg} / \mathrm{I}$ | 9.0 | 11.7 | 9.9 | 2.1 | 5.2 |
| Mn (total) | $\mathrm{mg} / \mathrm{/}$ | 1.3 | 1.3 | 1.1 | 1.1 | 1.2 |
| TSS | $\mathrm{mg} / \mathrm{l}$ | 260 | 432 | 423 | 110 | 186 |
| pH |  | 8.41 | 8.25 | NM | 8.32 | 8.11 |
| EC | $\mathrm{uS} / \mathrm{cm}$ | 1140 | 1200 | NM | 1180 | 1161 |
| T | ${ }^{\circ} \mathrm{C}$ | 10.5 | 14.9 | NM | 21.1 | 22.1 |
| VLS-Vaporl/liquid Separator Sample Port |  |  |  |  |  |  |

OWS-Oil/Water Separator Sample Port
AS-Air Stripper Sample Port
WATER QUALITY MONITORING

|  |  | xtract | Ilfiel | 6, 7, | and | 5, 6 |  |  |  | Extracti | ellfield | 2, 4, |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\overline{\text { VLS }}$ |  | VLS | VLS | VLS | VLS | VLS | VLS | VLS | VLS | VLS | VLS | VLS |
|  |  | 04/13/04 | 05/18/04 | 06/16/04 | 07/15/04 | 08/10/04 | 09/22/04 | 10/16/04 | 11/09/04 | 11/09/04 | 12/15/04 | 01/18/05 |
| MBTE | ppb | <10 | <10 | <10 | <10 | <10 | <10 | <10 | $<1$ | <250 | <10 | <10 |
| Benzene | ppb | 598 | 126 | 78.1 | 414.1 | 85.3 | 45.2 | 21.8 | 1.3 | 2552 | 253.5 | 99.9 |
| Toluene | ppb | 433 | 274 | 182.9 | 656.1 | 159.4 | 40.6 | 21.6 | <1 | 10090 | 786 | 194.4 |
| Ethylbenzene | ppb | 49 | 38.3 | 39.4 | 103.2 | 19.7 | <10 | <10 | $<1$ | 3371 | 163.8 | 33.6 |
| Xylenes (Total) | ppb | 772 | 1382 | 1386 | 1944 | 1289 | 836 | 408 | 26 | 24070 | 1175 | 382 |
| Phenols (Total) | ppb | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
| GRO (TPH) | mg/l | 6.2 | 5.1 | 4.3 | 8.0 | 4.7 | 4.0 | 2.0 | $<0.2$ | 189.1 | 9.1 | 2.8 |


| Effluent |  | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $04 / 13 / 04$ | $05 / 18 / 04$ | $06 / 16 / 04$ | $07 / 15 / 04$ | $08 / 10 / 04$ | $09 / 22 / 04$ | $10 / 16 / 04$ | $11 / 09 / 04$ | $11 / 09 / 04$ | $12 / 15 / 04$ | $01 / 18 / 05$ |
| MBTE | ppb | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | 2.2 | $<1$ | $<1$ |
| Benzene | ppb | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | 2.6 | 1.3 | $<1$ |
| Toluene | ppb | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | 4.2 | 3.9 | $<1$ |
| Ethylbenzene | ppb | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | 9.6 | 3.3 | $<1$ |
| Xylenes (Total) | ppb | $<3$ | $<3$ | $<3$ | $<3$ | $<3$ | $<3$ | $<3$ | $<3$ | 28.2 | 11 | $<3$ |
| Phenols (Total) | ppb | 27.2 | 23.6 | 22.1 | 22.2 | 21.6 | 15.7 | $<10$ | $<10$ | 71.7 | 175.0 | 98.6 |
| GRO (TPH) | $\mathrm{mg} / 1$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | 1.70 | 0.5 | $<0.2$ |


| Selected Parameters | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $04 / 13 / 04$ | $05 / 18 / 04$ | $06 / 16 / 04$ | $07 / 15 / 04$ | $08 / 10 / 04$ | $09 / 22 / 04$ | $10 / 16 / 04$ | $11 / 09 / 04$ | $11 / 09 / 04$ | $12 / 15 / 04$ | $01 / 18 / 05$ |
| Fe (total) | $\mathrm{mg} / \mathrm{I}$ | 7.1 | 1 | 0.68 | 0.8 | 2.34 | 2.88 | 0.42 | 0.49 | 8.05 | 2.76 | 0.98 |
| Mn (total) | $\mathrm{mg} / \mathrm{ll}$ | 0.74 | 0.5 | 0.44 | 0.41 | 0.53 | 0.54 | 0.36 | 0.36 | 0.56 | 0.66 | 0.37 |
| TSS | $\mathrm{mg} / \mathrm{l}$ | 76 | 105 | 11 | 17 | 122 | 126 | 2 | 3 | 125 | 80 | 40 |
| pH |  | 8.03 | 8.02 | 7.89 | 7.39 | 7.35 | 7.38 | 7.23 | 7.46 | 7.29 | 7.39 | 7.47 |
| EC | uS/cm | 1065 | 1059 | 1008 | 1123 | 1050 | 1036 | 1102 | 1023 | 1064 | 1050 | 1213 |
| T | ${ }^{\circ} \mathrm{C}$ | 9.9 | 12.8 | 16.42 | 16.91 | 16.32 | 16.30 | 13.73 | 11.1 | 11.3 | 10.2 | 10.6 |

WATER QUALITY MONITORING
Extraction wellfield HR 2, 3, and 4

Extraction wellfield HR 2, 4, and 5 | VLS | VLS | VLS | VLS | VLS | VLS | VLS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $07 / 11 / 05$ | $07 / 11 / 05$ | $08 / 02 / 05$ | $08 / 25 / 05$ | $09 / 13 / 05$ | $10 / 13 / 05$ | $11 / 22 / 05$ |
| $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<5$ | $<1$ |
| 108.3 | 1.4 | $<1$ | 8.5 | 6.7 | 102.8 | $<1$ |
| 157.1 | 1.7 | $<1$ | $<1$ | 1.4 | 10.2 | $<1$ |
| 17.2 | $<1$ | $<1$ | $<1$ | $<1$ | 8.2 | $<1$ |
| 330.8 | $<3$ | $<3$ | 16.3 | 7.2 | 28.6 | $<3$ |
| NA | NA | NA | NA | NA | NA | NA |
| 1.0 | $<0.2$ | $<0.2$ | 0.4 | $<0.2$ | $<0.2$ | $<0.2$ |

| Effluent |  | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent | Effluent |
| :--- | :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | $04 / 06 / 05$ | $04 / 19 / 05$ | $05 / 02 / 05$ | $06 / 13 / 05$ | $07 / 11 / 05$ | $07 / 11 / 05$ | $08 / 02 / 05$ | $08 / 25 / 05$ | $09 / 13 / 05$ | $10 / 13 / 05$ | $11 / 22 / 05$ |
| MBTE | ppb | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ |
| Benzene | ppb | 23.6 | 7.8 | 2.9 | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ |
| Toluene | ppb | 39.8 | 18.6 | 8 | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ |
| Ethylbenzene | ppb | 1.9 | 1.5 | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ |
| Xylenes (Total) | ppb | 28.5 | 19.4 | 9.4 | $<3$ | $<3$ | $<3$ | $<3$ | $<3$ | $<3$ | $<3$ | $<3$ |
| Phenols (Total) | ppb | 215.0 | 204.0 | 151 | 112.0 | 62.5 | $<10$ | $<10$ | 11.7 | $<10$ | 49.5 | 43.6 |
| GRO (TPH) | $\mathrm{mg} / \mathrm{l}$ | 0.39 | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ | $<0.2$ |


| Selected Parameters |  | $\begin{aligned} & \text { Effluent } \\ & 04 / 06 / 05 \end{aligned}$ | Effluent <br> 04/19/05 | $\begin{aligned} & \text { Effluent } \\ & 05 / 02 / 05 \end{aligned}$ | $\begin{aligned} & \text { Effluent } \\ & 06 / 13 / 05 \end{aligned}$ | Effluent <br> 07/11/05 | Effluent <br> 07/11/05 | $\begin{aligned} & \hline \text { Effluent } \\ & 08 / 02 / 05 \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 08 / 25 / 05 \end{aligned}$ | $\begin{aligned} & \text { Effluent } \\ & 09 / 13 / 05 \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 10 / 13 / 05 \end{aligned}$ | $\begin{aligned} & \hline \text { Effluent } \\ & 11 / 22 / 05 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fe (total) | $\mathrm{mg} / \mathrm{l}$ | 6.27 | 4.38 | 2.17 | 2.67 | 2.66 | 3.95 | 0.46 | 0.3 | 0.41 | 26.1 | 8.55 |
| Mn (total) | $\mathrm{mg} / \mathrm{l}$ | 1.14 | 0.81 | 0.81 | 0.82 | 0.49 | 0.49 | 0.14 | 0.4 | 0.42 | 1.51 | 0.66 |
| TSS | $\mathrm{mg} / \mathrm{l}$ | 145 | 116 | 39 | 29 | 55 | 79 | 33 | <1 | <1 | 405 | 14 |
| pH |  |  | 7.99 | 7.97 | 7.79 | 7.82 | 7.79 | 7.83 | 7.62 | 7.91 | 7.48 | 7.66 |
| EC | uS/cm |  | 1242 | 1241 | 1397 | 1121 | 1492 | 1134 | 1321 | 1140 | 1133 | 1124 |
| T | ${ }^{\circ} \mathrm{C}$ |  | 8.49 | 8.5 | 8.9 | 8.9 | 8.4 | 10.6 | 11.4 | 9.4 | 10.5 | 9.1 |

## APPENDIX G-2

## OFFGAS QUALITY

Organic Vapors By Charcoal Tube Desorption, Summit Analyzer, Flame Ionization Detector, and Photo Ionization Detector Data represent combined VOC concentrations for specific extraction wellfield.

| Date/Time | Collection Interval | Sampling Flow Rate (L/min) | $\begin{aligned} & \text { GRO } \\ & \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{aligned}$ | $\begin{gathered} \text { TPH } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{gathered} \text { MTBE } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | Benzene $\left(\mathrm{mg} / \mathrm{m}^{3}\right)$ | Toluene ( $\mathrm{mg} / \mathrm{m}^{3}$ ) | $\begin{gathered} \text { Ethyl } \\ \text { benzene } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \\ \hline \end{gathered}$ | Xylenes <br> $\left(\mathrm{mg} / \mathrm{m}^{3}\right)$ | Summit (ppm) | $\begin{aligned} & \text { FID } \\ & \text { (ppm) } \end{aligned}$ | $\begin{gathered} \text { PID } \\ \text { (ppm) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7/11/02 14:05 | CT-30 s | 0.20 | 99,600 | 218,000 | ND | 4,810 | 1,630 | ND | ND | OL | OL | OL |
| 7/11/02 14:07 | CT-15 s | 0.20 | 146,000 | 332,000 | ND | 7,320 | 1,630 | ND | ND |  |  |  |
| 7/16/02 18:30 | CT-30 s | 0.20 | 30,800 | 73,500 | ND | 1,800 | 631 | ND | ND | OL | OL | 1,910 |
| 7/16/02 18:35 | CT-15 s | 0.20 | 28,100 | 68,400 | ND | 1,580 | 446 | ND | ND |  |  |  |
| 9/18/02 9:45 | CT-30 s | 0.28 | 53,400 | 97,800 | ND | 1,890 | 2,310 | 150 | 493 | OL | OL | OL |
| 9/18/02 9:47 | CT-30 s | 0.28 | 56,100 | 98,800 | ND | 1,990 | 2,750 | 193 | 650 |  |  |  |
| 9/24/02 15:40 | CT-30 s | 0.28 | 38,400 | 58,900 | ND | 1,090 | 1,640 | 79 | 247 | OL | OL | 2,355 |
| 10/2/02 14:05 | CT-30 s | 0.28 | 26,700 | 40,900 | ND | 767 | 571 | ND | 51 | 8,907 | 45,000 | 2,000 |
| 10/2/02 14:07 | CT-30 s | 0.28 | 31,000 | 45,200 | ND | 943 | 914 | 39 | 138 |  |  |  |
| 10/16/02 12:15 | CT-60 s | 0.28 | 13,000 | 19,200 | ND | 233 | 318 | 21 | 143 | 5,800 | 15,000 | 800 |
| 10/16/02 12:17 | CT-60 s | 0.28 | 14,200 | 20,500 | ND | 157 | 261 | 21 | 138 |  |  |  |
| 11/18/02 16:03 | CT-30 s | 0.28 | 2,240 | 4,390 | ND | 74 | 20 | ND | ND | 3,395 | 7,800 | 1,283 |
| 11/18/02 16:05 | CT-60 s | 0.28 | 6,710 | 9,070 | ND | 211 | 138 | 4.9 | 30 |  |  |  |
| 11/18/02 16:07 | CT-60 s | 0.28 | 6,890 | 9,180 | ND | 224 | 174 | 7.3 | 48 |  |  |  |
| 11/18/02 16:15 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 6,070 | 8,290 | ND | 175 | 111 | 3.5 | 24 |  |  |  |
| 12/16/02 14:54 | CT-60 s | 0.28 | 6,440 | 8,620 | ND | 139 | 101 | 3.3 | 18 | 2,480 | 3,800 | 273 |
| 12/16/02 14:54 | CT-60 s | 0.28 | 6,000 | 8,370 | ND | 177 | 130 | 4.2 | 25 |  |  |  |
| 1/7/03 12:47 | CT-60 s | 0.28 | 4,200 | 6,040 | ND | 135 | 86 | ND | 8.5 | 2,005 | 3,040 | 270 |
| 1/7/03 12:49 | CT-60 s | 0.28 | 4,850 | 6,610 | ND | 166 | 138 | 4.8 | 24 |  |  |  |

[^3]OFFGAS QUALITY MONITORING (Continued)

| Date/Time | Collection Interval | Sampling Flow Rate (L/min) | $\begin{gathered} \text { GRO } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{gathered} \text { TPH } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{aligned} & \text { MTBE } \\ & \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{aligned}$ | $\begin{gathered} \text { Benzene } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \\ \hline \end{gathered}$ | Toluene $\left(\mathrm{mg} / \mathrm{m}^{3}\right)$ | Ethyl benzene $\left(\mathrm{mg} / \mathrm{m}^{3}\right)$ | Xylenes <br> ( $\mathrm{mg} / \mathrm{m}^{3}$ ) | Summit (ppm) | $\begin{gathered} \text { FID } \\ (\mathrm{ppm}) \\ \hline \end{gathered}$ | $\begin{gathered} \text { PID } \\ \text { (ppm) } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3/28/03 11:00 | CT-30 s | 0.28 | 32,400 | 65,200 | ND | 590 | 309 | 11 | ND | 12,755 | OL | OL |
| 3/28/03 11:02 | CT-30 s | 0.28 | 18,000 | 37,700 | ND | 276 | 90 | ND | ND | 12,755 | OL | OL |
| 3/28/03 11:05 | ${ }^{1}$ CT-30 s | 0.28 | 74,100 | 144,000 | ND | 1,790 | 2,020 | 216 | 1100 |  |  |  |
| 4/23/03 10:10 | CT-60 s | 0.28 | 6,230 | 8,220 | ND | 157 | 134 | 4.9 | 29 | 2,342 | 3,500 | 1,470 |
| 4/23/03 10:12 | CT-60 s | 0.28 | 6,670 | 8,690 | ND | 163 | 204 | 11 | 66 |  |  |  |
| 5/19/03 13:58 | CT-60 s | 0.28 | 2,100 | 2,810 | ND | 63 | 17 | ND | ND | 1,515 | 2,264 | 1,470 |
| 5/19/03 14:00 | CT-60 s | 0.28 | 4,490 | 5,500 | ND | 146 | 81 | 2 | ND |  |  |  |
| 6/17/03 15:10 | CT-60 s | 0.28 | 1,960 | 2,280 | ND | 90 | 36 | ND | 5.6 | 811 | 1,350 | 560 |
| 6/17/03 15:12 | CT-60 s | 0.28 | 2,650 | 2,960 | ND | 126 | 86 | ND | 20 |  |  |  |
| 7/15/03 17:20 | CT-60 s | 0.28 | 1,680 | 2,170 | ND | 53 | 46 | ND | 4.5 | 783 | 901 | 507 |
| 7/15/03 17:22 | CT-60 s | 0.28 | 1,660 | 2,150 | ND | 64 | 53 | ND | 7.6 |  |  |  |
| 7/22/03 13:28 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 4,540 | 6,240 | ND | 34 | 52 | ND | 4.6 | 710 | 3,870 | 1,200 |
| 7/22/0313:30 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 5,610 | 7,750 | ND | 48 | 101 | 3.3 | 18 |  |  |  |
| 8/21/03 9:44 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 8,180 | 10,500 | ND | 115 | 175 | 4.2 | 11 | 5,620 | 10,000 | 1,540 |
| 8/21/03 9:45 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 9,500 | 11,900 | ND | 150 | 300 | 12 | 35 |  |  |  |
| 9/23/03 17:50 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 9,480 | 12,300 | ND | 185 | 294 | 6.4 | 15 | 5,015 | 3,875 | 1,571 |
| 9/23/03 17:55 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 11,100 | 13,900 | ND | 221 | 568 | 20 | 65 |  |  |  |
| 10/22/03 15:26 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 3,350 | 4,320 | ND | 33 | 48 | ND | 5.9 | data set | 3,330 | 1,599 |
| 10/22/03 15:32 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 4,720 | 5,990 | ND | 124 | 289 | 11 | 68 | data set |  |  |
| 11/17/03 16:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 345 | 501 | ND | 22 | 20 | ND | 5.1 | Malfunctir | 1,140 | 920 |
| 11/17/03 16:05 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 358 | 515 | ND | 24 | 29 | ND | 11 | Malfunctio |  |  |
| 12/17/03 16:33 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 1,640 | 2,180 | ND | 19 | ND | ND | ND | 1513 | 1,720 | 777 |
| 12/17/03 16:36 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND |  |  |  |

OFFGAS QUALITY MONITORING (Continued)

|  | Collection | $\begin{aligned} & \text { Sampling } \\ & \text { Flow Rate } \end{aligned}$ | (mq/m) |  |  | Berzene | ${ }_{\text {Toluene }}^{\substack{\text { Tolug } \\(m g m)}}$ | $\begin{gathered} \text { Ethyl } \\ \text { benzene } \\ \left(\mathrm{mg} / \mathrm{m}^{2}\right) \end{gathered}$ | Xylenes |  |  | $\stackrel{\text { PlD }}{\text { (pom) }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Daterime }}{41230412.07}$ | ${ }_{\text {Interval }}$ | $\frac{(L / 2 m i n)}{0.28}$ | $\frac{\left(\mathrm{mg} / \mathrm{m}^{3}\right)}{3,70}$ | $\frac{\left(\mathrm{mg} / \mathrm{m}^{\text {s }} \text { ) }\right.}{11,000}$ |  | $\frac{(m g / m)}{49}$ | $\frac{\left(\mathrm{mg} / \mathrm{m}^{3}\right)}{13}$ | ${ }_{\text {(mg }}^{\text {No }}$ ) | ${ }_{\text {(mg/m }}$ |  |  |  |
| 423304 12:22 | 'ct-60 | ${ }_{0}$ | ${ }_{3,500}$ | 9,710 |  | 45 | 17 | ND | ND |  |  |  |
| 51/8049:59 | 'ct | 0.28 | 1,160 | 1,470 | ND | 11 | 10 | ND | ND | 720 | 820 | 350 |
| 5/1804 |  | 0.28 | 1,510 | 1,890 | ND | 15 |  |  |  |  |  |  |
| 06616/04 14:40 | ${ }^{\text {'ct-60 }}$ | 0.28 | 1140 | 1260 | ND | 12 | 20 | ND | ${ }_{5} .3$ | 539 | 195 | 452 |
| 06/16/04 14:42 | 'ct-60 | 0.28 | 1270 | 1390 | ND | 11 | 26 | ND | 21 |  |  |  |
| 7/15004 10:32 | 'ст | 0.28 | 9420 | 21300 | ND | 72 | 70 | 4.6 | ${ }^{24}$ | 999 | 500 | 1657 |
| 71/5/0416:34 |  | 0.28 |  |  | ND | 84 | 87 |  |  |  |  |  |
| 8/10/0415.40 | 'CT-60 s | 0.28 | 1100 | 1590 | ND | 7.8 | ${ }^{9.6}$ | ND | 4.5 | 1050 | 624 | 567 |
| 8/10004 15:42 | 'CT-60 s | 0.28 | 1190 | 1700 | ND | ${ }^{9.6}$ | 11 | ND |  |  |  |  |
| 9/22/04 14:15 | 'ct-60 s | 0.28 | 265 | 340 | ND | 0.89 | 0.93 | ${ }^{6.6}$ | 7.8 | 587 | 562 | 475 |
| 9/22/04 14:15 | ${ }^{\text {'ct-60s }}$ | 0.28 | 354 | 443 | ND | 1 | 1.4 | 11 | 13 |  |  |  |
| 1016/104 19:30 |  | 0.28 | 1350 | 1690 | ND | 4.2 | ND | 37 |  | 530 | 392 | mal |
| 10116/04 19:30 | 'CT-60 s | 0.28 | 1460 | 1830 | ND | 4 | ND | ${ }^{37}$ | 45 |  |  |  |
| 1119/048:35 | ${ }^{\prime} \mathrm{CT}$-60 s | 0.28 | ND | ND | ND | ND | ND | 0.94 | 0.72 | 2100 | 88 | 99.1 |
| 11190048:35 | 'CT-60 s | 0.28 | ND | ND | ND | ND | ND | ${ }^{0.84}$ | ND |  |  |  |
| 1119004 16:05 |  | 0.28 |  |  |  |  |  |  | 32 | 4920 | 10,0 | 1927 |
| 11/904 16:05 | 'CT-60 s | 0.28 | 1720 | 2970 | ND | 45 | ${ }^{65}$ | 7 | 34 |  |  |  |
| 121/5/04 23:15 | 'ct-60 s | 0.28 | 1390 | 1820 | ND | 35 | 100 | ${ }^{20}$ | ${ }^{92}$ |  |  |  |
| 12115/04 23:30 | 'CT-60 s | 0.28 | 1220 | 1620 | ND | 32 |  |  |  |  |  |  |
| 1118/0500:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ${ }_{6}^{6.8}$ | ND | 4.8 | ${ }^{96}$ | 189 | 251 |
| 11/18050:00 | 'ct-60 s | 0.28 | ND | ND | ND | ND | ND |  |  |  |  |  |

OFFGAS QUALITY MONITORING (Continued)

| Date/Time | Collection Interval | Sampling Flow Rate (L/min) | $\begin{gathered} \text { GRO } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{gathered} \text { TPH } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{gathered} \text { MTBE } \\ \left(\mathrm{mg} / \mathrm{m}^{3}\right) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Benzene } \\ & \left(\mathrm{mg} / \mathrm{m}^{3}\right) \end{aligned}$ | Toluene $\left(\mathrm{mg} / \mathrm{m}^{3}\right)$ | Ethyl benzene $\left(\mathrm{mg} / \mathrm{m}^{3}\right)$ | Xylenes $\left(\mathrm{mg} / \mathrm{m}^{3}\right)$ | Summit (ppm) | $\begin{aligned} & \text { FID } \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{gathered} \text { PID } \\ \text { (ppm) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4/6/05 8:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 389 | 1900 | ND | 39 | 74 | 3.1 | 24 | 3558 | 13342 | 3358 |
| 4/6/05 8:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 2880 | 7170 | ND | 146 | 281 | 16 | 99 |  |  |  |
| 4/19/05 18:10 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND | 2246 | 1252 | 932 |
| 4/19/05 18:10 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 1600 | 2690 | ND | 69 | 168 | 10 | 72 |  |  |  |
| 5/2/05 14:40 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 1420 | 1690 | ND | 26 | 61 | 15 | 18 | 511 | 965 | 382 |
| 5/2/05 14:40 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND |  |  |  |
| 6/13/05 14:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 670 | 780 | ND | 20 | 63 | 9.3 | 55 | 211 | 425 | 279 |
|  | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 547 | 673 | ND | 22 | 59 | 9.3 | 59 |  |  |  |
| 7/11/05 14:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 288 | 311 | ND | 18 | 30 | 3.8 | 34 | 96 | 275 | 99 |
|  | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | 312 | 340 | ND | 20 | 33 | 4.4 | 44 |  |  |  |
| 7/11/05 16:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | 0.59 | 4.5 | 57 | 131 | 74 |
|  | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND |  |  |  |
| 8/2/05 12:30 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND | 18 | 71 | 15 |
|  | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND |  |  |  |
| 8/25/05 14:15 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND | 9 | 12.7 | 36.1 |
|  | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND |  |  |  |
| 9/13/05 17:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | 2.2 | ND | ND | ND | 74 | 49 | 121 |
|  | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | 4.6 | ND | ND | ND |  |  |  |
| 10/13/05 14:00 | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | ND | ND | ND | ND | 1830 | 1172 | NM |
|  | ${ }^{1} \mathrm{CT}-60 \mathrm{~s}$ | 0.28 | ND | ND | ND | 32 | 3.4 | ND | 6 |  |  |  |
| 11/22/05 14:00 | System shutdown |  | No samples collected with respect to ND in previous sampling events |  |  |  |  |  |  | NM | 0 | 0 |


[^0]:    
    
     741.32
    739.12
    
     1741.62 1742.10
    1741.45
     1742.25

     $\stackrel{\text { in }}{\stackrel{0}{+}}$号 | 8 |
    | :--- |
    | 0 |
    | 0 |

    $1740.78 \quad 1741.34 \quad 1741.03$ 1740.35 $\qquad$ $\stackrel{N}{N}$

    $$
    \begin{aligned}
    & 1740.20 \\
    & 1741.60
    \end{aligned}
    $$ 1742.31

    1741.53

    $$
    \begin{aligned}
    & 1741.37 \\
    & 1739.91
    \end{aligned}
    $$ 1740.16 1743.19 1741.16 0

    $\stackrel{0}{0}$
    $\stackrel{y}{ \pm}$ $\stackrel{N}{\stackrel{N}{+}}$ 1741.24 $\stackrel{N}{\stackrel{N}{J}}$
    
    

    $$
    \sum_{i} \frac{N}{N}
    $$ 둗

    \subsection*{1740.55 <br> 1740.55} $\stackrel{\Omega}{\stackrel{\Omega}{\alpha}}$ 1742.60 | MW-1 | 1751.06 | 1753.85 | 1753.90 | 1742.21 | 1740.08 | 1740.27 | 1740.57 |
    | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
    | MW-2 | 1751.08 | 1750.47 | 1750.56 | 1742.18 | 1739.36 | 1740.03 | 1740.21 |
    | MW-3 | 1752.35 | 1751.63 | 1751.70 | 1742.31 | 1742.10 | 1741.93 | 1741.90 |
    | MW-4 | 1752.12 | 1754.50 | 1754.50 | 1742.66 | 1742.60 | 1742.61 | 1742.50 |
    | MW-5 | 1749.03 | 1751.69 | 1751.69 | 1742.07 | 1741.88 | 1741.92 | 1741.92 |
    | MW-6 | 1744.17 | 1746.46 | 1746.46 | 1741.73 | 1741.69 | 1742.19 | 1740.13 |
    | MW-7 | 1753.22 | 1753.03 | 1753.03 | 1742.68 | 1742.70 | 1742.50 | 1742.55 |
    | MW-8 | 1751.14 | 1753.39 | 1753.39 | 1742.19 | 1742.09 | 1741.97 | 1742.02 |
    | MW-9 | 1749.78 | 1749.20 | 1749.20 | 1742.13 | 1742.14 | 1741.45 | 1741.58 |
    | MW-10 | 1749.29 | 1750.59 | 1750.59 | 1742.10 | 1737.91 | 1738.74 | 1739.23 |
    | MW-11 | 1751.79 | 1751.16 | 1751.25 | 1742.29 | 1742.10 | 1741.90 | 1742.00 |
    | MW-12 | 1751.60 | 1751.08 | 1751.21 | 1742.22 | 1741.96 | 1741.81 | 1741.84 |
    | MW-13 | 1751.18 | 1750.52 | 1750.59 | 1742.20 | 1741.63 | 1741.37 | 1741.39 |
    | MW-14 | 1751.49 | 1750.78 | 1750.87 | 1742.18 | 1741.52 | 1741.28 | 1741.37 |
    | MW-15 | 1751.11 | 1750.51 | 1750.64 | 1742.19 | 1741.17 | 1741.14 | 1741.29 |
    | MW-16 | 1745.68 | 1745.48 | 1745.48 | 1743.21 | 1742.88 | 1741.35 | 1741.28 |
    | MW-17 | 1745.01 | 1744.96 | 1744.96 | 1739.36 | 1738.31 | 1739.55 | 1739.72 |

    MP1 - measuring point after wellhead instrumentation

[^1]:    1740.63
    

[^2]:    

[^3]:    ND - Not Detected
    NM - Not Measured
    OL=Overloaded
    $>10,000 \mathrm{ppmv}$ for Summit (calibrated on hexane) $>10,000 \mathrm{ppmv}$ for PID (calibrated on isobuthylene) - $\mathbf{5 0 , 0 0 0} \mathrm{ppmv}$ for FID (calibrated on methane)
    ${ }^{1}$ Charcoal tube sample collected from tedlar bag
    GRO - Gasoline Range Organics
    TPH - Total Purgeable Hydrocarbons
    CT - Charcoal Tube
    TB - Tedlar Bag
    FID - Flame Ionization Detector
    PID - Photoionization Detector
    Summit - Summit HydrocarbonAnalyzer

